DEVELOPING CLOSURES FOR TURBULENT FLOW OF VISCOELASTIC FENE-P FLUIDS

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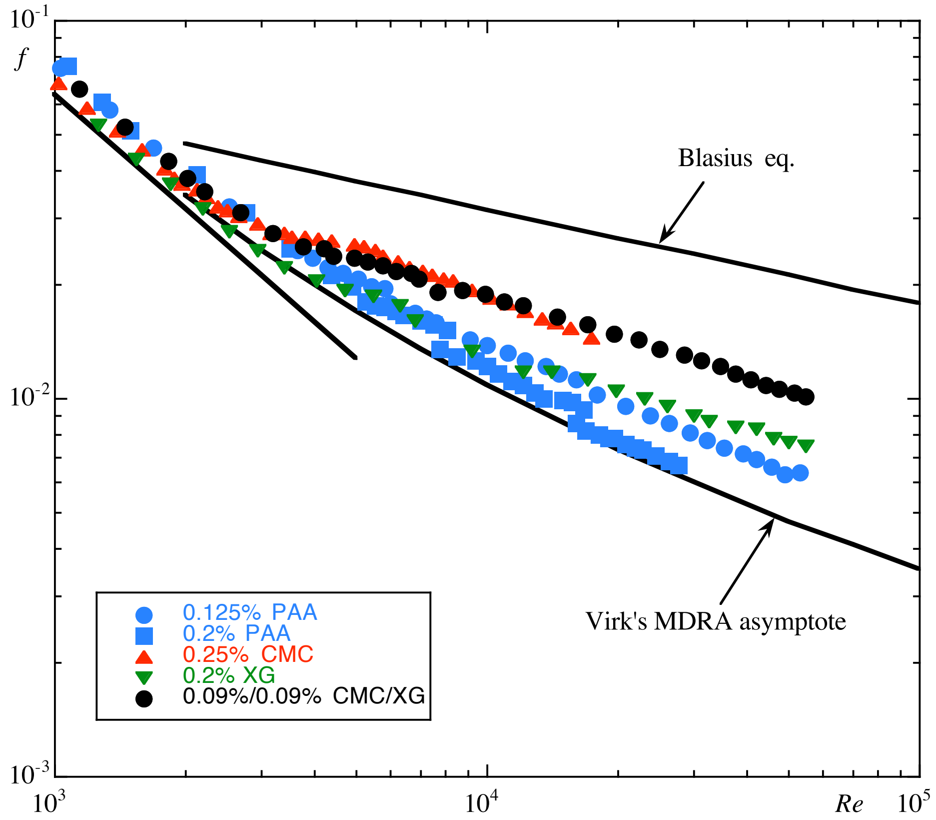
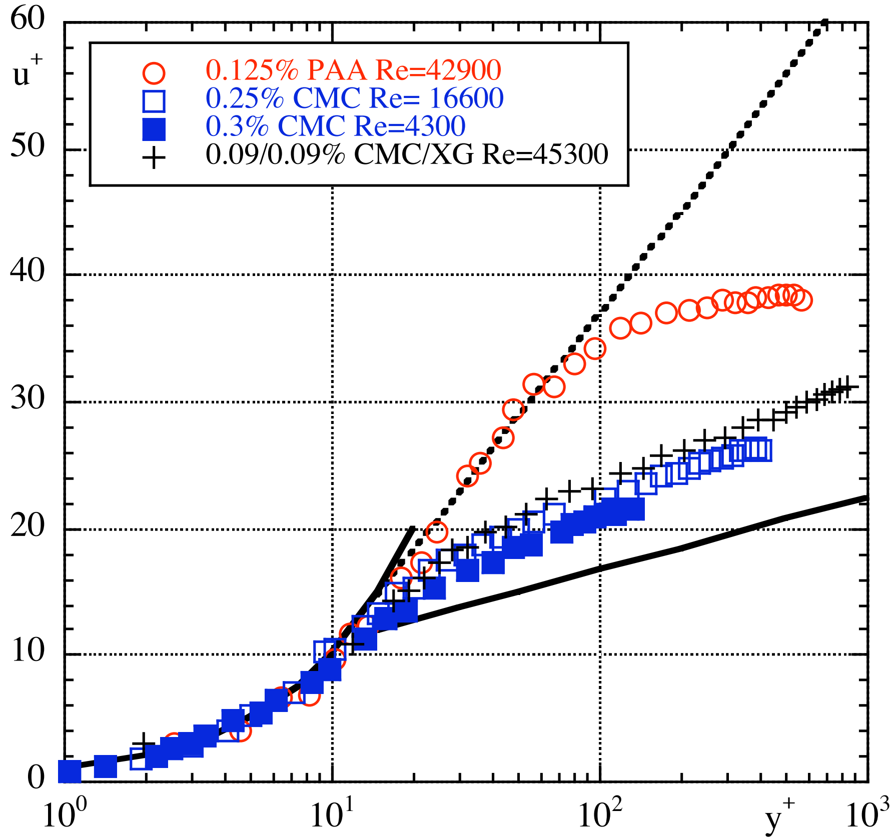
Summary

- Relevance: some facts about drag reduction
- Governing equations for FENE-P in RANS form
- Reynolds decomposition of FENE-P equations
- Closure needs and analysis of DNS case (LDR)
- A simplified closure with *a priori* testing of DNS data
- Some concerns regarding limiting cases
- Some preliminary results
- Conclusions

Relevance: drag reduction in turbulent pipe flow





Escudier et al JNNFM (1999)

- Reduction of shear Reynolds stress (DR)
- Increase of normal streamwise Reynolds stress
- Dampening of normal radial and tangential Reynolds stress

Deficit of Reynolds stress

Time-average governing equations: turbulent flow & FENE-P

^- instantaneous
Overbar or capital letter- time-average
` or small letter- fluctuations

Continuity: $$\frac{\partial U_i}{\partial x_i}=0$$

Momentum balance:

$$\rho\frac{\partial U_i}{\partial t}+\rho U_k\frac{\partial U_i}{\partial x_k}=-\frac{\partial \overline{p}}{\partial x_i}+\eta_s\frac{\partial^2 U_i}{\partial x_k \partial x_k}-\frac{\partial}{\partial x_k}\left(\rho\overline{u_i u_k}\right)+\frac{\partial \overline{\tau}_{ik,p}}{\partial x_k}$$

$$\overline{\tau}_{ij}=2\eta_s S_{ij}+\overline{\tau}_{ij,p}$$

Rheological constitutive equation: **FENE-P**

$$\hat{\tau}_{ij,p}=\frac{\eta_p}{\lambda}\left[f\left(\hat{C}_{kk}\right)\hat{C}_{ij}-f\left(L\right)\delta_{ij}\right]$$

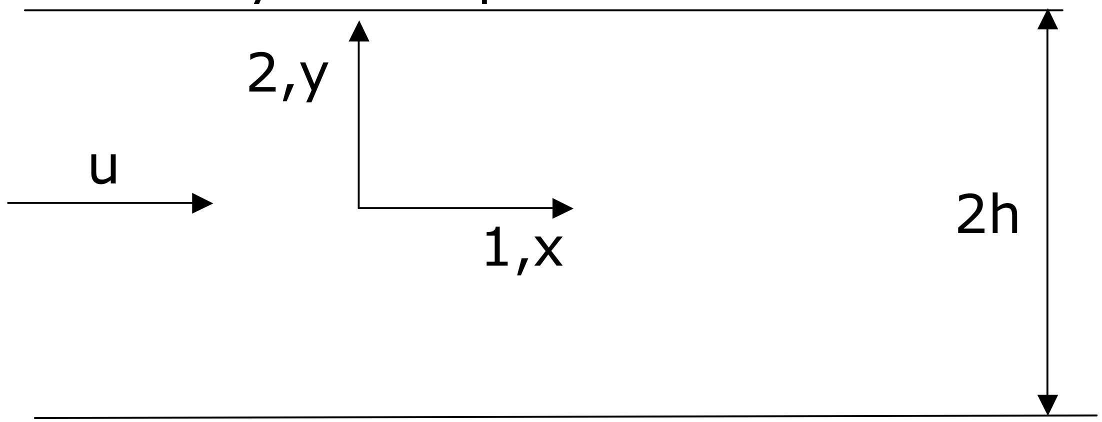
$$f\left(\hat{C}_{kk}\right)\hat{C}_{ij}+\lambda\left(\frac{\partial \hat{C}_{ij}}{\partial t}+\hat{U}_k\frac{\partial \hat{C}_{ij}}{\partial x_k}-\hat{C}_{jk}\frac{\partial \hat{U}_i}{\partial x_k}-\hat{C}_{ik}\frac{\partial \hat{U}_j}{\partial x_k}\right)=f(L)\delta_{ij}$$

$$\left(\frac{\partial \hat{C}_{ij}}{\partial t}+\hat{U}_k\frac{\partial \hat{C}_{ij}}{\partial x_k}-\hat{C}_{jk}\frac{\partial \hat{U}_i}{\partial x_k}-\hat{C}_{ik}\frac{\partial \hat{U}_j}{\partial x_k}\right)=\overset{\nabla}{\hat{C}}_{ij}=-\frac{\hat{\tau}_{ij,p}}{\eta_p}$$

DNS case: LDR

DNS, DR=18% (LDR)

Fully-developed channel flow



$$We_\tau = 25, Re_\tau = 395$$
$$\beta = 0.9, L^2 = 900$$

$$We_\tau = \frac{\lambda u_\tau^2}{\nu_0} \qquad Re_\tau = \frac{h u_\tau}{\nu_0}$$

Reynolds decomposition of conformation tensor

$$\hat{B} = B + b' \quad \text{where} \quad \overline{b'} = 0$$

Function: $f\left(C_{kk}\right) = \dfrac{L^2 - 3}{L^2 - C_{kk}}$

Time average polymeric stress

$$\overline{\tau}_{ij,p} = \frac{\eta_p}{\lambda}\left[f\left(C_{kk}\right)C_{ij} - f\left(L\right)\delta_{ij}\right] + \frac{\eta_p}{\lambda}\overline{f\left(C_{kk}+c_{kk}\right)c_{ij}}$$

$$\overline{f' c_{ij}}$$

Neglected (see slide)

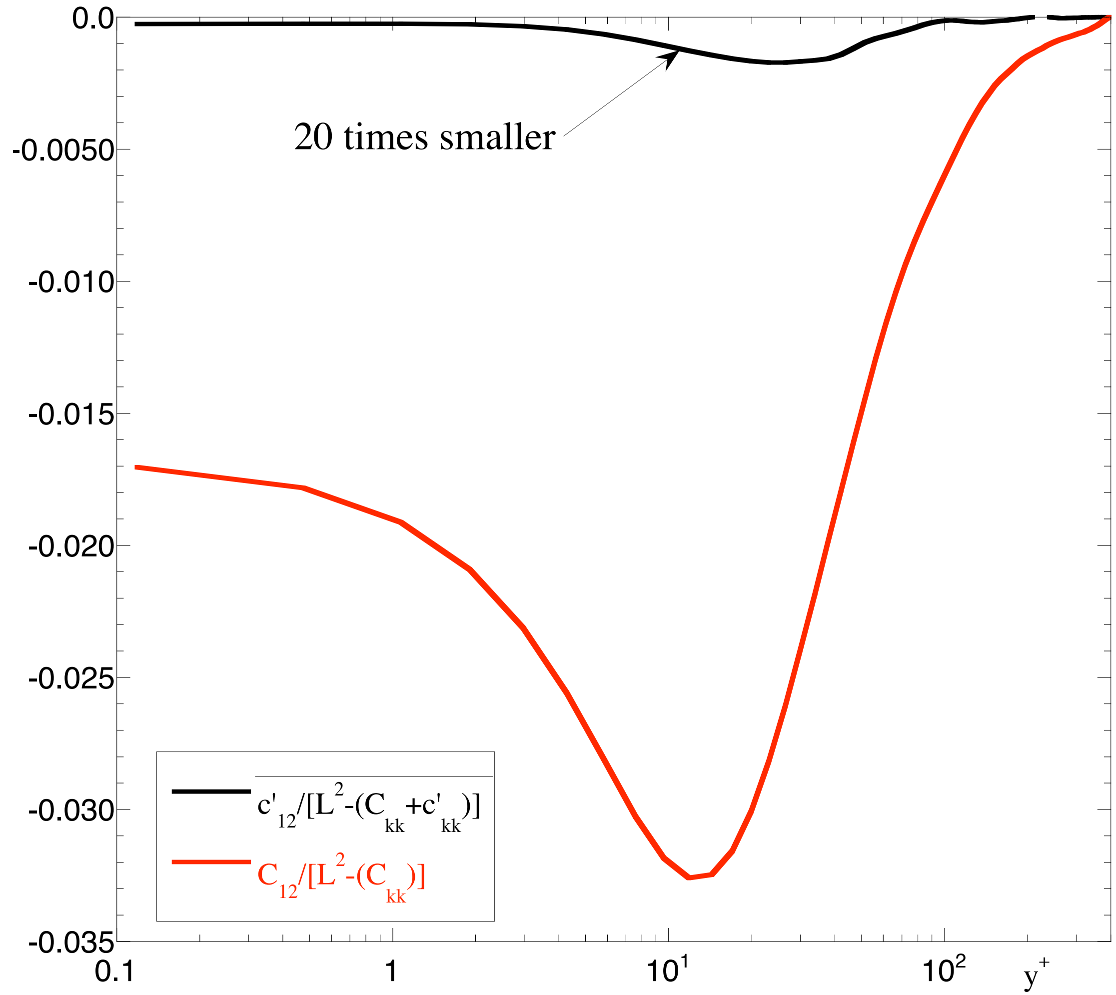
Time average conformation tensor equation

$$\lambda \overset{\nabla}{C}_{ij} + \lambda\left[\overline{u_k \frac{\partial c_{ij}}{\partial x_k}} - \left(\overline{c_{kj}\frac{\partial u_i}{\partial x_k}} + \overline{c_{ik}\frac{\partial u_j}{\partial x_k}}\right)\right] = -\left[f\left(C_{kk}\right)C_{ij} - f\left(L\right)\delta_{ij} + \overline{f\left(C_{kk}+c_{kk}\right)c_{ij}}\right]$$

$$\overset{\nabla}{C}_{ij} + \overline{u_k \frac{\partial c_{ij}}{\partial x_k}} - \left(\overline{c_{kj}\frac{\partial u_i}{\partial x_k}} + \overline{c_{ik}\frac{\partial u_j}{\partial x_k}}\right) = -\frac{\overline{\tau}_{ij,p}}{\eta_p}$$

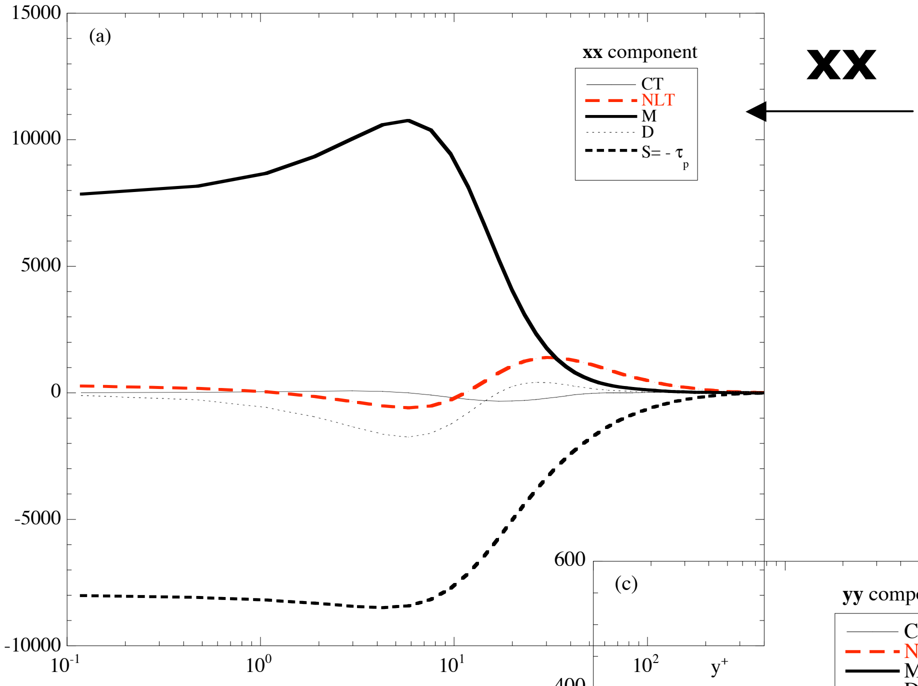
CT_{ij} $\quad$ NLT_{ij}

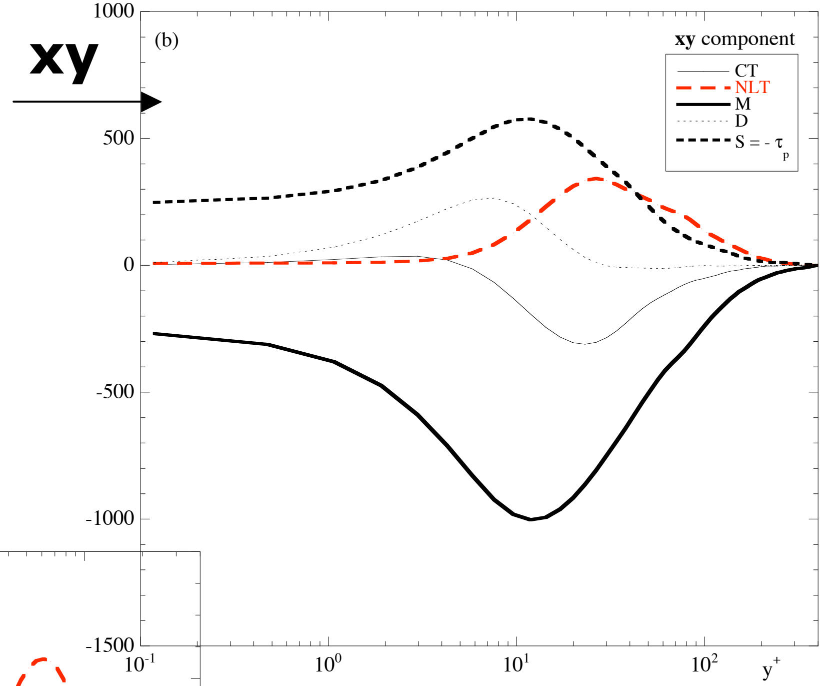
Simplifying assumptions: justification from DNS

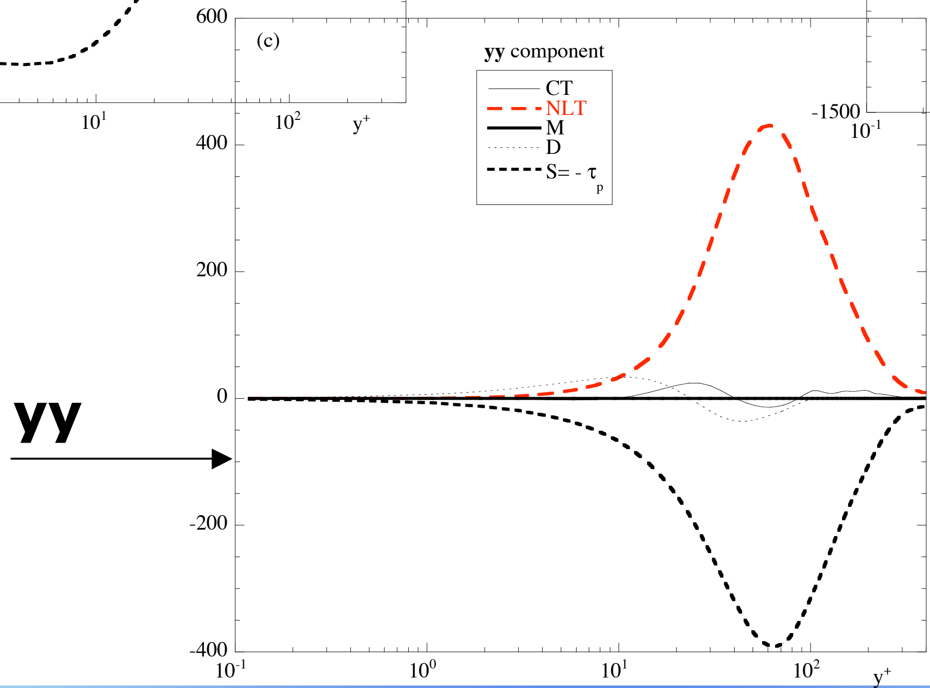


$$f\left(C_{kk}\right)C_{12} >> \overline{f' c_{12}} = \overline{f\left(C_{kk}+c_{kk}^{'}\right)c_{12}^{'}} = \left(L^2-3\right)\overline{\frac{c_{12}^{'}}{L^2-\left(C_{kk}+c_{kk}^{'}\right)}}$$

Polymer stress







Housiadas et al (2005)
Li et al (2006) JNNFM

Modeling requirements

$$\frac{\overline{\tau}_{ij,p}}{\eta_p} = -\overset{\nabla}{C}_{ij} - \overline{u_k \frac{\partial c_{ij}}{\partial x_k}} + \left(\overline{c_{kj}\frac{\partial u_i}{\partial x_k}} + \overline{c_{ik}\frac{\partial u_j}{\partial x_k}} \right)$$

$\overset{\nabla}{C}_{ij} \rightarrow M_{ij}$

NLT_{ij}: originates in Oldroyd derivative
not negligible, must be modeled

CT_{ij} : originates in advective term, it is negligible
no need for modeling

DNS: Housiadas et al (2005), Li et al (2006) JNNFM

What about:

1) Reynolds stresses?

2) Turbulent kinetic energy ?

3) Dissipation of turbulent kinetic energy or of Reynolds stresses ?

Transport equation for the Reynolds stresses and *k*

$$\rho\frac{\partial\overline{u_i u_j}}{\partial t}+\rho U_k\frac{\partial\overline{u_i u_j}}{\partial x_k}=P_{ij}+Q_{ij}+Q_{ij}^V+D_{ij,N}+\Pi_{ij}-\rho\varepsilon_{ij}^N-\rho\varepsilon_{ij}^V$$

$$Q_{ij}^V=\frac{\partial}{\partial x_k}\left(\overline{u_i\tau'_{jk,p}}+\overline{u_j\tau'_{ik,p}}\right)$$

Viscoelastic turbulent transport due to fluctuations polymeric stresses

$$\varepsilon_{ij}^V=\frac{1}{\rho}\left(\overline{\tau'_{jk,p}\frac{\partial u_i}{\partial x_k}}+\overline{\tau'_{ik,p}\frac{\partial u_j}{\partial x_k}}\right)$$

Viscoelastic work of polymer chains: dissipation of energy plus stored free energy (<0 ou >0)

$$\rho\frac{Dk}{Dt}+\rho\overline{u_i u_k}\frac{\partial U_i}{\partial x_k}=-\rho\overline{u_i\frac{\partial k'}{dx_i}}-\frac{\partial\overline{p'u_i}}{\partial x_i}+\eta_s\frac{\partial^2 k}{\partial x_i\partial x_i}-\eta_s\overline{\frac{\partial u_i}{\partial x_k}\frac{\partial u_i}{\partial x_k}}+\frac{\partial\overline{\tau'_{ik,p}u_i}}{\partial x_k}-\overline{\tau'_{ik,p}\frac{\partial u_i}{\partial x_k}}$$

ε^N $\quad Q^V$ $\quad \varepsilon^V$

Transport equation of ε^N

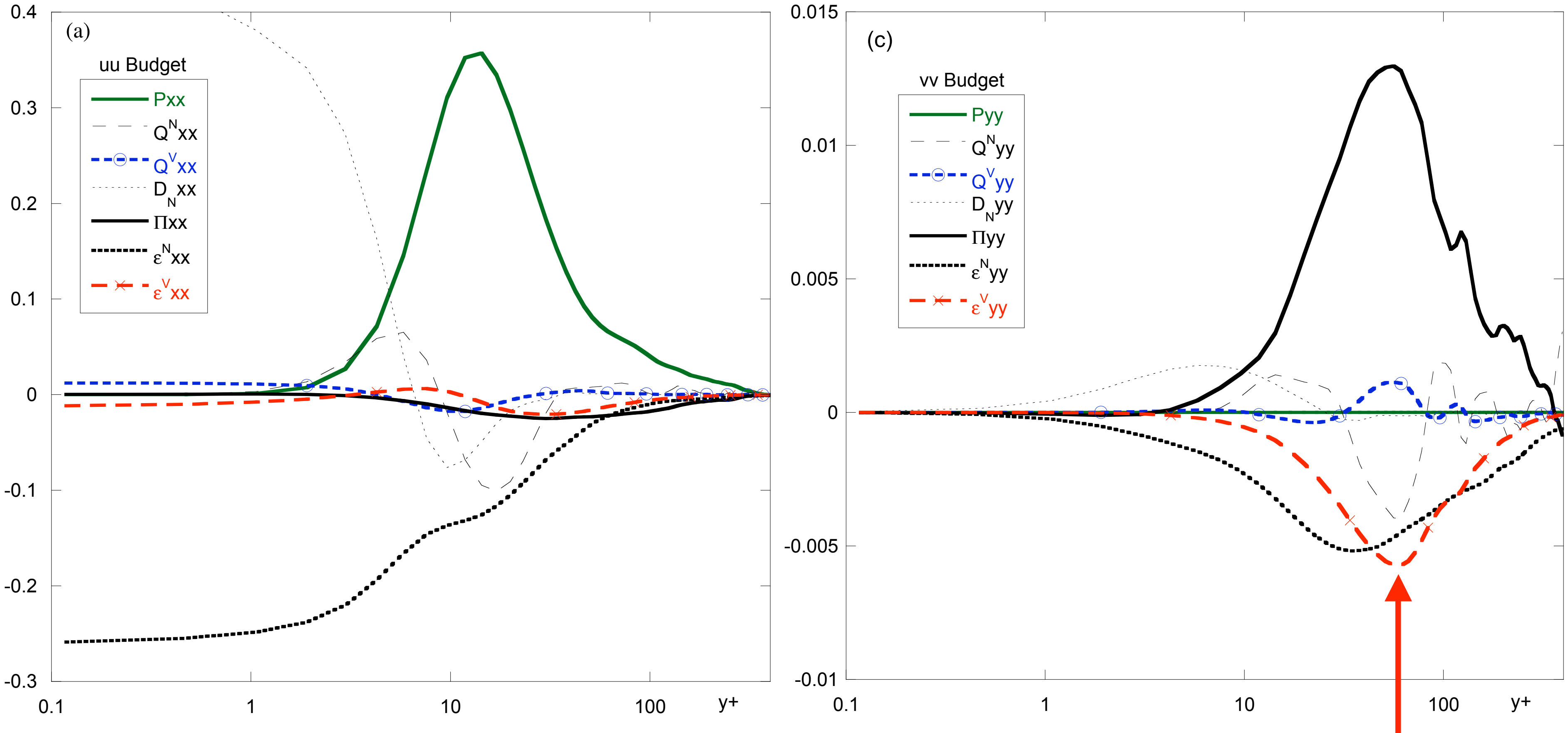
$$2\nu_s \overline{\frac{\partial u_i}{\partial x_m}\frac{\partial}{\partial x_m}\left(\rho\frac{Du_i}{Dt}\right)} + 2\nu_s \overline{\frac{\partial u_i}{\partial x_m}\frac{\partial}{\partial x_m}\left(\rho u_k\frac{\partial U_i}{\partial x_k}\right)} + 2\nu_s \overline{\frac{\partial u_i}{\partial x_m}\frac{\partial}{\partial x_m}\left(\rho\frac{\partial u_i u_k}{\partial x_k}\right)}$$

$$+2\nu_s \overline{\frac{\partial u_i}{\partial x_m}\frac{\partial}{\partial x_m}\left(\frac{\partial p'}{\partial x_i}\right)} - 2\rho\nu_s^2 \overline{\frac{\partial u_i}{\partial x_m}\frac{\partial}{\partial x_m}\left(\frac{\partial^2 u_i}{\partial x_k^2}\right)} - 2\nu_s \overline{\frac{\partial u_i}{\partial x_m}\frac{\partial}{\partial x_m}\left(\frac{\partial \tau'_{ik,p}}{\partial x_k}\right)} = 0$$

New term

As for Newtonian fluids, the whole equation will be approximated

Budget of Reynolds stress



- Need to model viscoelastic stress work
- Need to model pressure strain (effect of elasticity)- Advanced mod.

- Viscoelastic turbulent transport is not so important

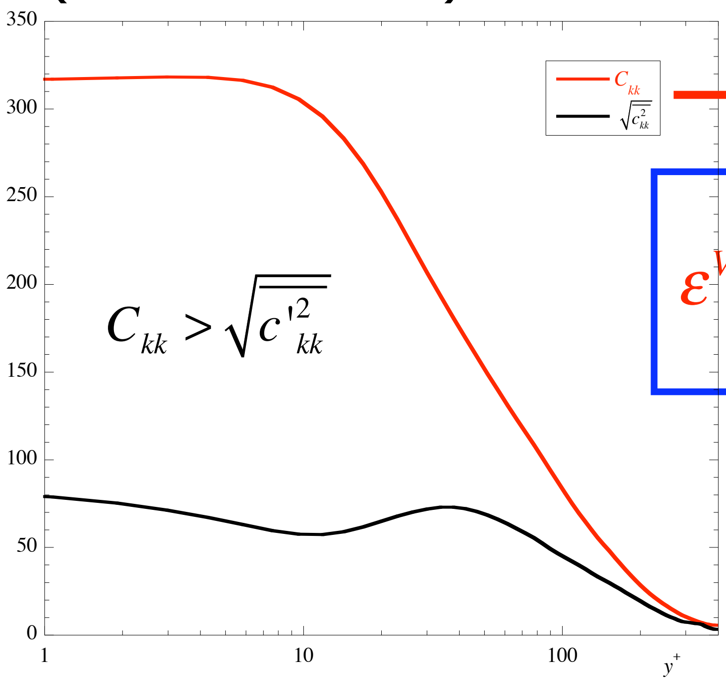
Viscoelastic work

$$\varepsilon^V \equiv \frac{1}{\rho}\overline{\tau'_{ik,p}\frac{\partial u_i}{\partial x_k}} = \frac{\eta_p}{\rho\lambda}\left[C_{ik}\overline{f(C_{mm}+c_{mm})\frac{\partial u_i}{\partial x_k}} + \overline{c_{ik}f(C_{mm}+c_{mm})\frac{\partial u_i}{\partial x_k}}\right]$$

Assumption:

(same reasons)

$$C_{ik}\overline{f(C_{mm}+c_{mm})\frac{\partial u_i}{\partial x_k}} < \overline{c_{ik}f(C_{mm}+c_{mm})\frac{\partial u_i}{\partial x_k}}$$



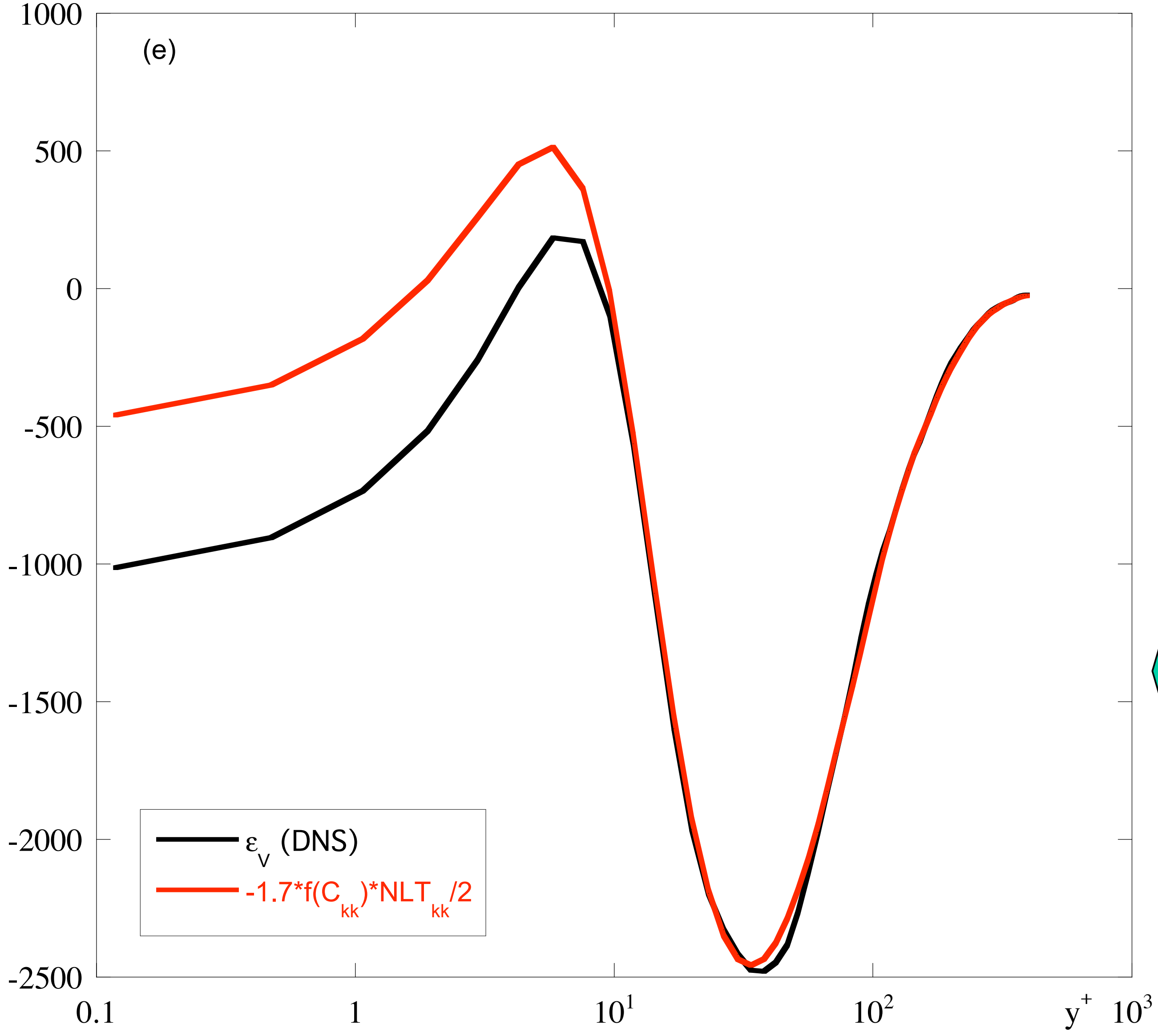
$$\varepsilon^V \approx \frac{\eta_p}{\rho\lambda} f(C_{mm})\overline{c_{ik}\frac{\partial u_i}{\partial x_k}} = C_{\varepsilon^V}\frac{\eta_p}{\rho\lambda} f(C_{mm})\frac{NLT_{nn}}{2}$$

Needs model

$C_{\varepsilon^V} = 1.076$

(from DNS- next slide)

Performance of the viscoelastic work model



$\varepsilon^V > 0$

Negative sign:
different
definitions

$\varepsilon^{V+}\left(\mathrm{Re}_{\tau_0}\right)^2$

versus

$f\left(C_{kk}\right)NLT_{ij}^*$

Modeling NLT_{ij} 1

Key ideas:

1) Write down exact equation- complex 4 lines long
2) Get inspiration from it: physical insight, trial-and-error, luck
3) Make assumptions
4) Do *a priori* testing of each term
5) Select appropriate combination and dimensional homogeneity
6) Try in code - under investigation

$$\overline{u_i u_m \frac{\partial c_{kj}}{\partial x_m}} + \overline{u_i u_m}\frac{\partial C_{kj}}{\partial x_m} \approx Coef \times \overline{u_i u_m}\frac{\partial C_{kj}}{\partial x_m}$$

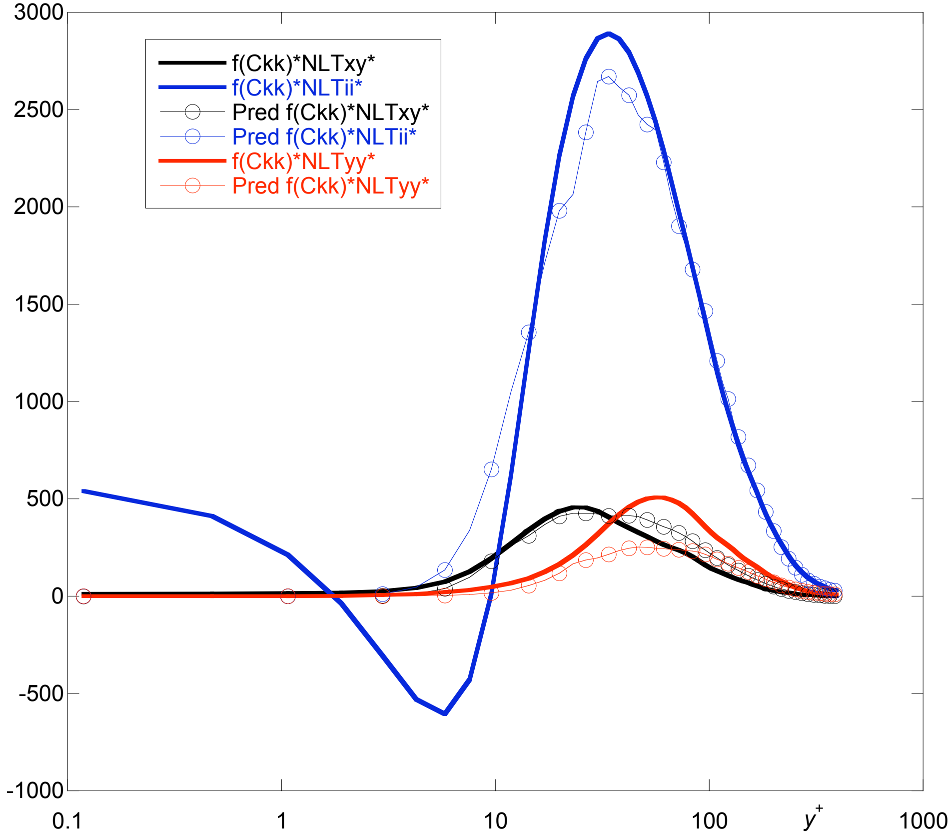
$$f(C_{mm})\frac{NLT_{ij}}{\lambda} = function\left(S_{ij}, W_{ij}, C_{ij}, \varepsilon_{ij}^{N}, \frac{\partial \overline{u_i u_j}}{\partial x_k}, \frac{\partial C_{ij}}{\partial x_k}, \frac{\partial NLT_{ij}}{\partial x_n}, M_{ij}, \overline{u_i u_j} \right)$$

$$f(C_{mm})\frac{NLT_{ij}}{\lambda} = f_{\mu_1}\left[C_{\gamma_1}\frac{\partial \overline{u_k u_n}}{\partial x_n}\frac{\partial C_{ij}}{\partial x_k} + \frac{C_{E_3} u_\tau^2}{\nu_0^2} C_{kk}\overline{u_i u_j} + \frac{C_{\alpha_{14}}}{\nu_0}\left(\overline{u_i u_k} W_{kn} C_{nj} + \overline{u_j u_k} W_{kn} C_{ni} + \overline{u_k u_i} W_{jn} C_{nk} \right) \right]$$

Model for NLT_{ij} 2

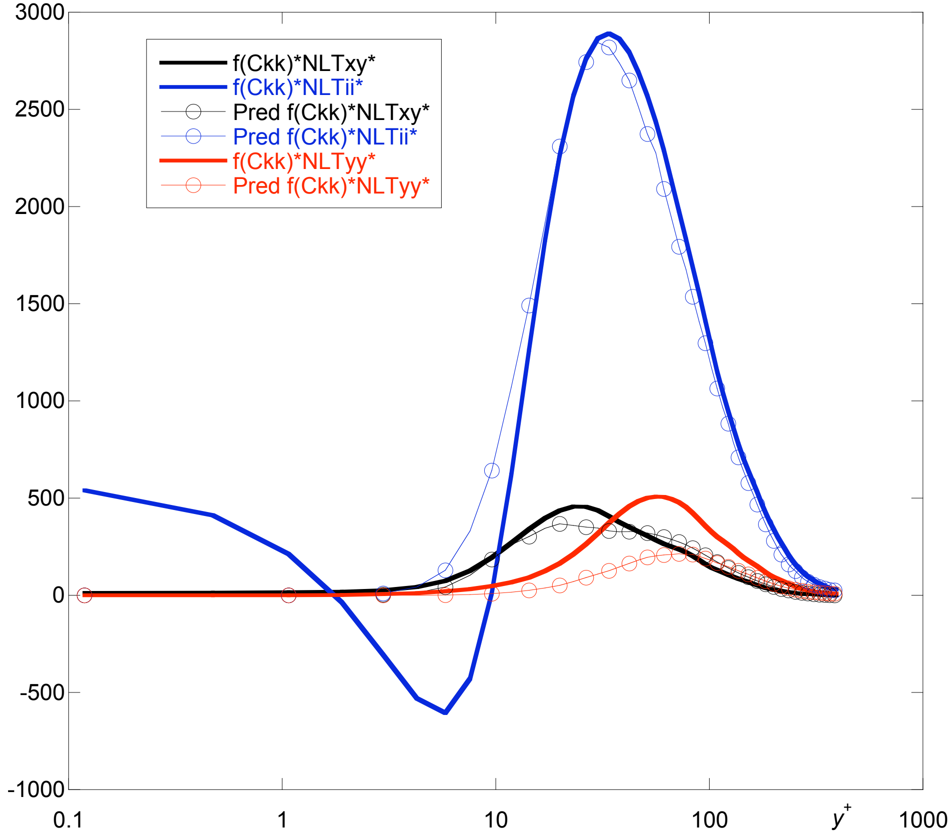
Blue model

$$C_{E_3} = 0.0004; C_{\gamma_1} = 3; C_{\alpha_{14}} = 0.00015$$



Red model

$$C_{E_3} = 0.00035; C_{\gamma_1} = 0; C_{\alpha_{14}} = 0.00015$$



$$f_{\mu_1} = \left(1 - \exp\left(-y^+/26.5\right)\right)^2$$

Viscoelastic turbulent transport

$$Q^V \equiv \frac{\partial \overline{\tau'_{ik,p} u_i}}{\partial x_k} = \frac{\eta_p}{\lambda} \frac{\partial}{\partial x_k} \left[C_{ik} \overline{f\left(C_{mm} + c_{mm}\right) u_i} + \overline{c_{ik} f\left(C_{mm} + c_{mm}\right) u_i} \right]$$

$$C_{kk} > \sqrt{\overline{c'^2_{kk}}}$$

$$f\left(\hat{C}_{mm}\right) = \frac{L^2 - 3}{L^2 - \left(C_{mm} + c_{mm}\right)}$$

Weak coupling between c_{kk} and c_{ij}, u_i

$$C_{ik} \overline{f\left(C_{mm} + c_{mm}\right) u_i} < \overline{c_{ik} f\left(C_{mm} + c_{mm}\right) u_i}$$

Neglect of this term is irrelevant because non-neglected term is modeled

$$Q^V = \frac{\eta_p}{\lambda} \frac{\partial}{\partial x_k} \left[f\left(C_{mm}\right) CU_{iik} \right]$$

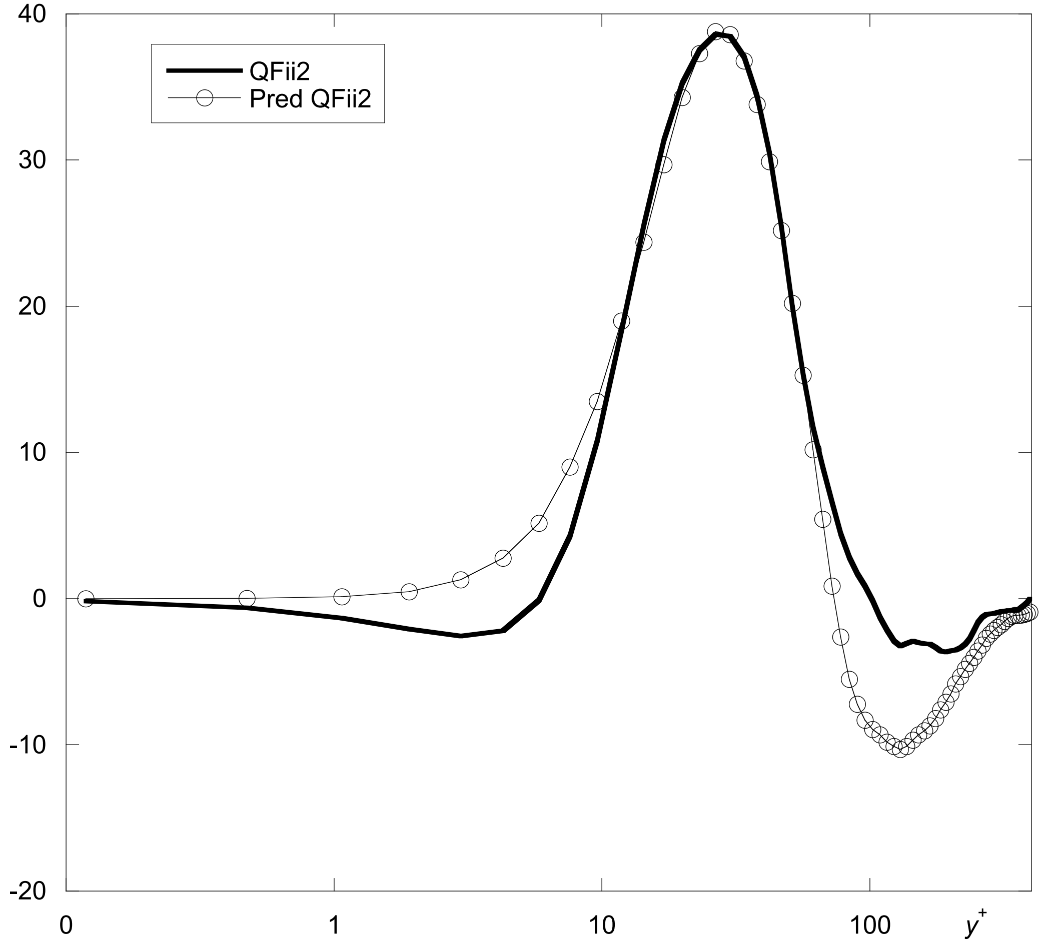
Needs model

General case $\left(CU_{ijk}\right)$

Model for CU_{ijk}

- Same modelling approach as with NLT_{ij}

$$\frac{f(C_{mm})CU_{ijk}}{\lambda} = f_{\mu_2}\left[-C_{\beta_1}\left(\overline{u_i u_m}\frac{\partial C_{kj}}{\partial x_m} + \overline{u_j u_m}\frac{\partial C_{ik}}{\partial x_m}\right) - \frac{C_{\beta_7}}{\lambda} f(C_{mm})\left[\pm\sqrt{\overline{u_j^2}}C_{ik} \pm \sqrt{\overline{u_i^2}}C_{jk}\right]\right]$$



$$C_{\beta_1} = 1.3; C_{\beta_7} = 0.37$$

$$f_{\mu_2} = 1 - \exp\left(-\frac{y^+}{26.5}\right)$$

Final equations: low *Re* *k*-ε type model for channel flow

Momentum:

$$\frac{d}{dy}\left[\eta_s \frac{dU}{dy} + \overline{\tau}_{p,xy} - \rho\overline{uv}\right] - \frac{d\overline{p}}{dx} = 0$$

$$\overline{\tau}_{xy,p} = \frac{\eta_p}{\lambda} f\left(C_{kk}\right) C_{xy}$$

$$f\left(C_{kk}\right) C_{xy} = \lambda C_{yy} \frac{dU}{dy} + \lambda NLT_{xy}$$

$$f\left(C_{kk}\right) C_{yy} = \lambda NLT_{yy} + 1$$

$$f\left(C_{kk}\right) C_{xx} = 2\lambda C_{xy} \frac{dU}{dy} + \lambda NLT_{xx} + 1$$

$$f\left(C_{kk}\right) C_{zz} = \lambda NLT_{zz} + 1$$

$$f\left(C_{kk}\right) = \frac{L^2 - 3}{L^2 - \left(C_{xx} + C_{yy} + C_{zz}\right)}$$

Reynolds stress:

$$-\rho\overline{uv} = \rho\nu_T \frac{dU}{dy} \quad \text{with} \quad \nu_T = C_\mu f_\mu \frac{k^2}{\tilde{\varepsilon}^N}$$

k and ε transport equations

$$0=\frac{d}{dy}\left[\left(\eta_s+\frac{\rho\nu_T}{\sigma_k}\right)\frac{dk}{dy}\right]+P_k-\rho\tilde{\varepsilon}^N-\rho D+\eta_p\frac{d}{dy}\left[\frac{f(C_{mm})}{\lambda}\frac{CU_{nny}}{2}\right]-\eta_p\frac{f(C_{mm})}{\lambda}\frac{NLT_{nn}}{2}$$

$$\varepsilon^N=\tilde{\varepsilon}^N+D^N \qquad D^N=2\eta_s\left(\frac{d\sqrt{k}}{dy}\right)^2$$

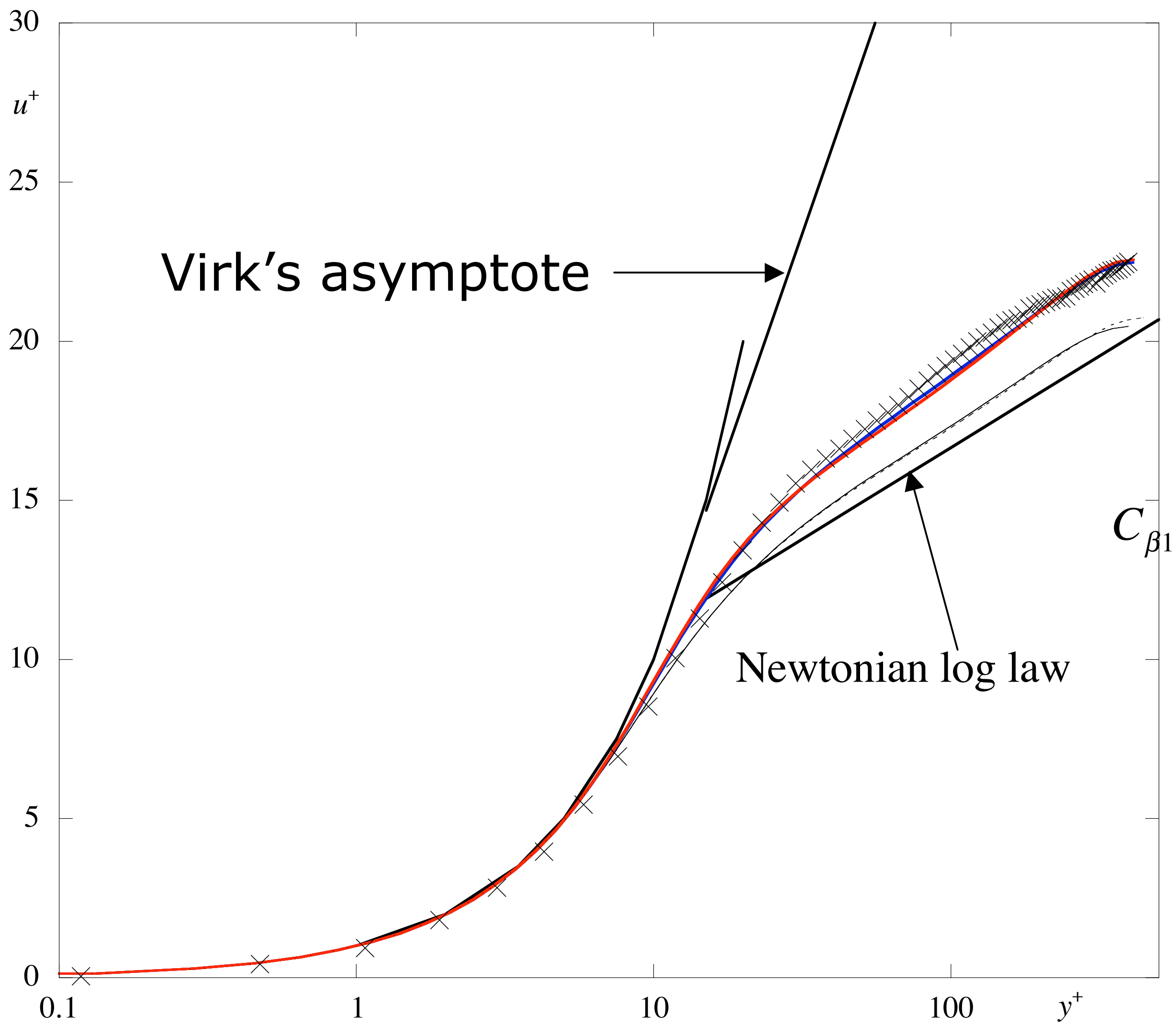
$$0=\frac{d}{dy}\left[\left(\eta_s+\frac{\rho\nu_T}{\sigma_\varepsilon}\right)\frac{d\tilde{\varepsilon}^N}{dy}\right]+\rho f_1 C_{\varepsilon_1}\frac{\tilde{\varepsilon}^N}{k}\frac{P_k}{\rho}-\rho f_2 C_{\varepsilon_2}\frac{\varepsilon^{N^2}}{k}+\rho E+E_{\tau_p}$$

$$E=\frac{\eta_s}{\rho}\nu_T\left(1-f_\mu\right)\left(\frac{d^2U}{dy^2}\right)^2$$

$$f_1=1 \qquad f_2=1-0.3\exp\left(-R_T^2\right) \qquad f_\mu=\left[1-\exp\left(\frac{-y^+}{26.5}\right)\right]^2$$

based on Newtonian model of Nagano & Hishida (1984)

Some results 1: $Re_{\tau 0}$= 395; $We_{\tau 0}$= 25; β=0.9, L^2=900



X DNS

Black: Newtonian

——— $\eta = \eta_s + \eta_p$

— — — $\eta = \eta_{wall}$

- - - - - - - $\eta = \eta_{wall}; \text{same } \dot{Q}; Re_{\tau_0} = 443$

FENE-P simulations

$$C_{\beta 1} = 1.3; C_{\beta 7} = 0.37; C_{\alpha 14} = 1.5 \times 10^{-4}$$

$$C_{\varepsilon^V} = 1.076$$

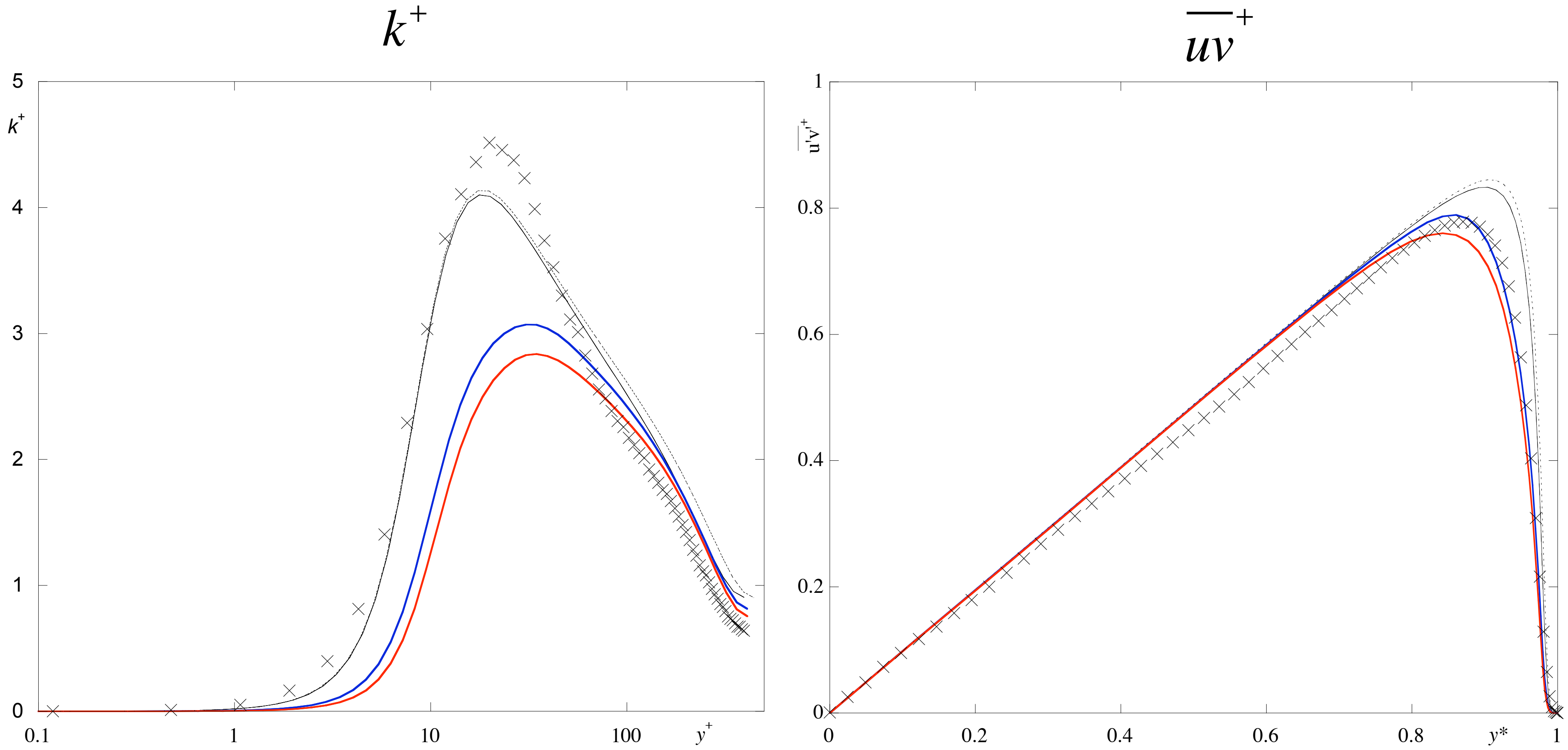
With ε^p

——— $C_{E3} = 1.93 \times 10^{-4}$

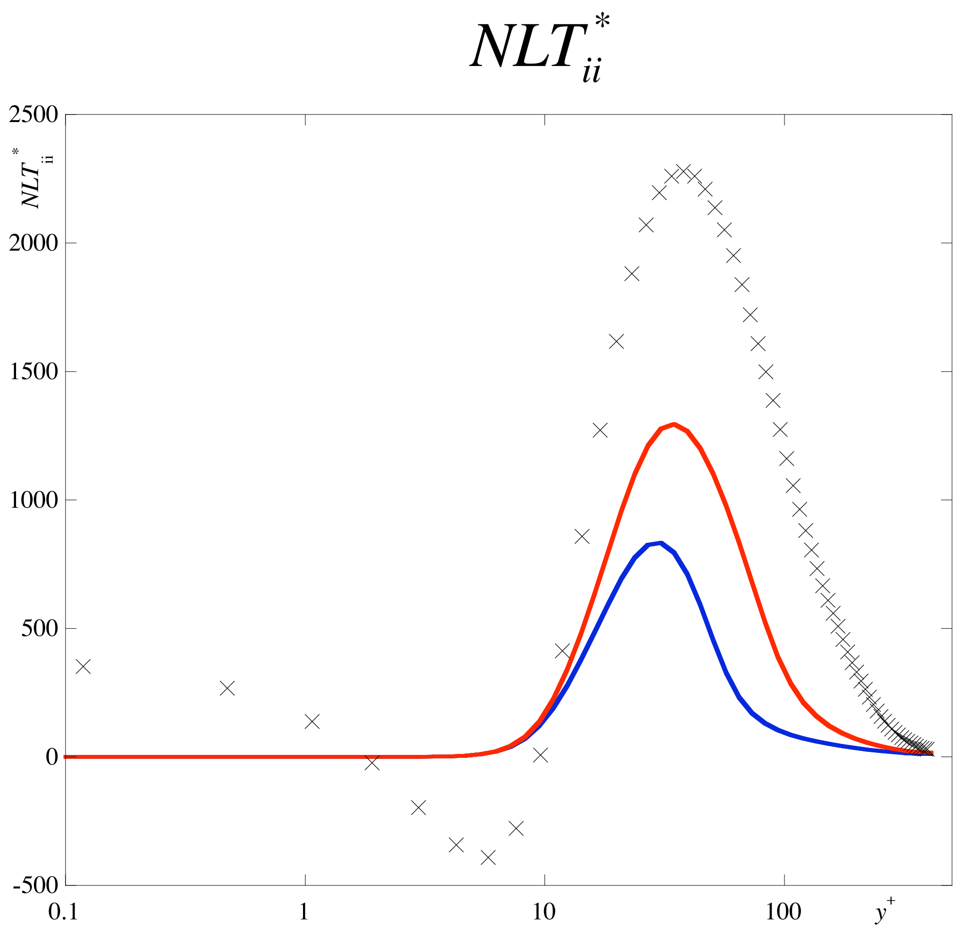
Without ε^p

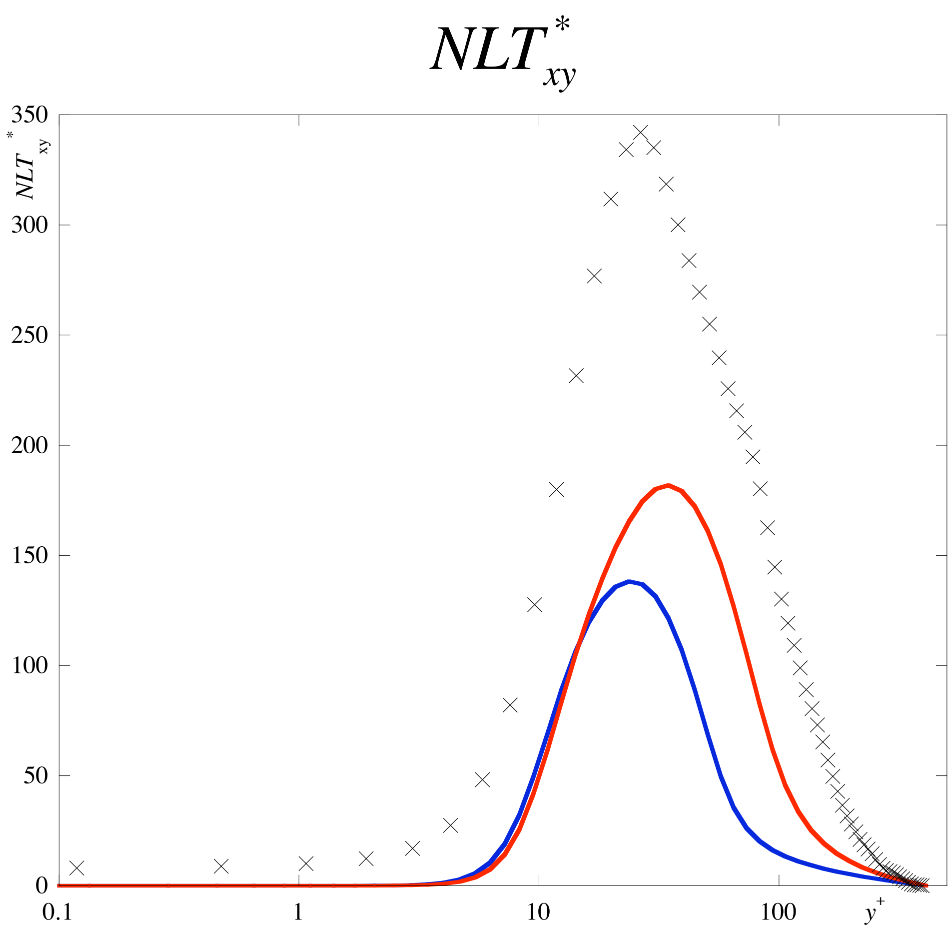
——— $C_{E3} = 2.86 \times 10^{-4}$

Some results 2: $Re_{\tau 0}$= 395; $We_{\tau 0}$= 25; β=0.9, L^2=900

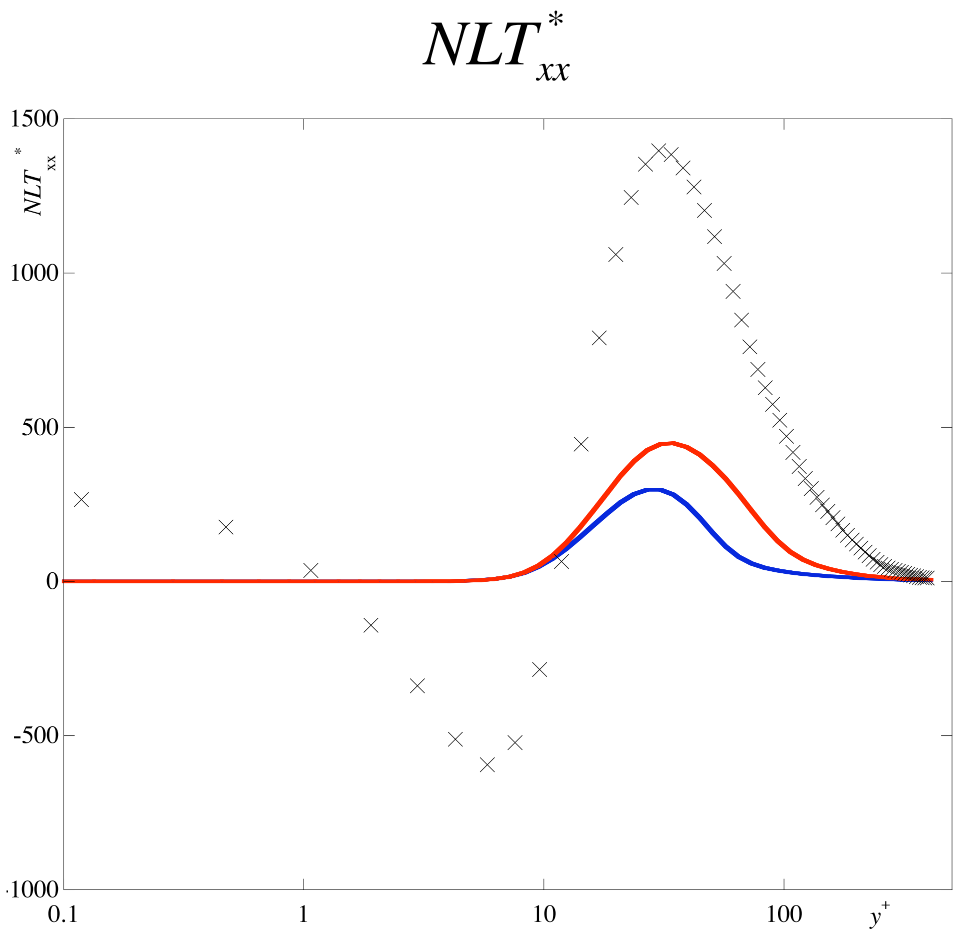


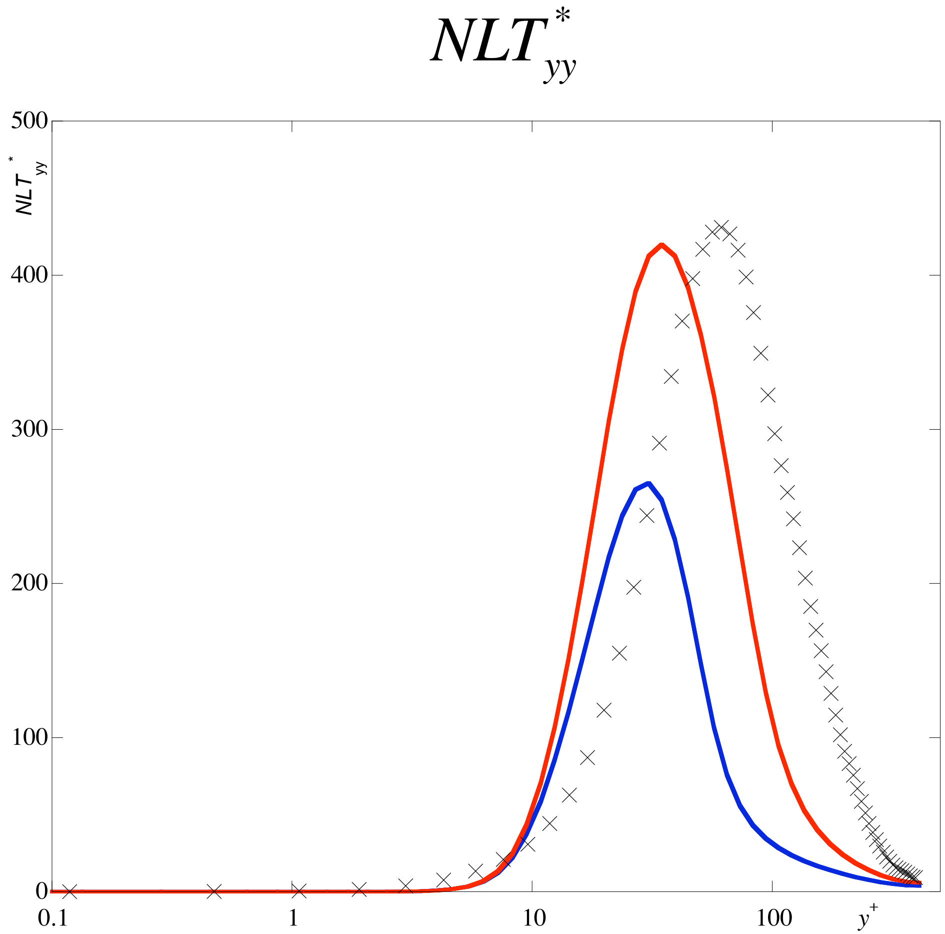
Some results 3: $Re_{\tau 0}$= 395; $We_{\tau 0}$= 25; β=0.9, L^2=900



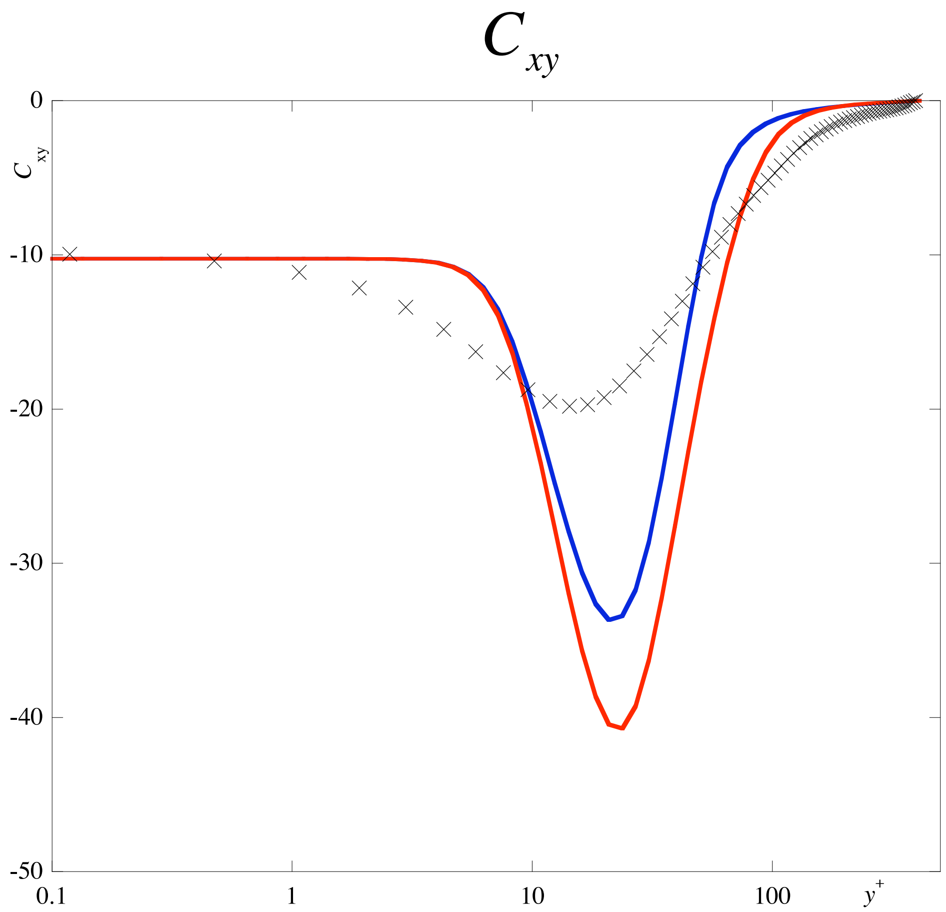


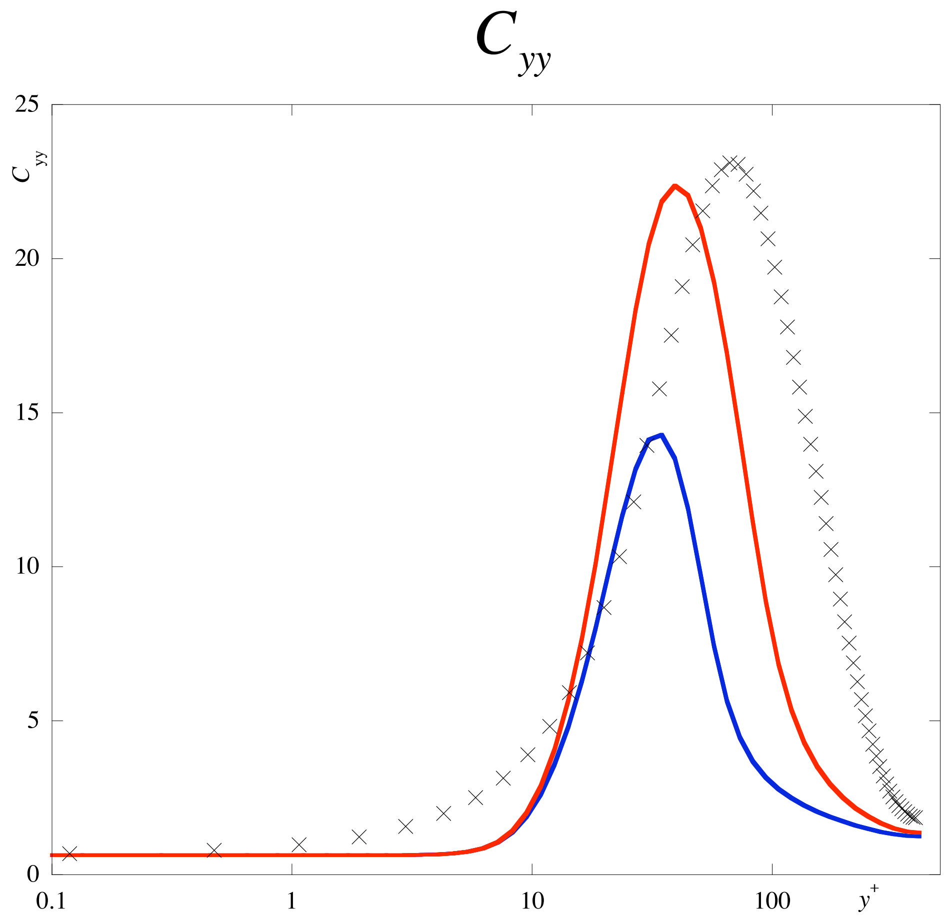
Some results 4: $Re_{\tau 0}$= 395; $We_{\tau 0}$= 25; β=0.9, L^2=900



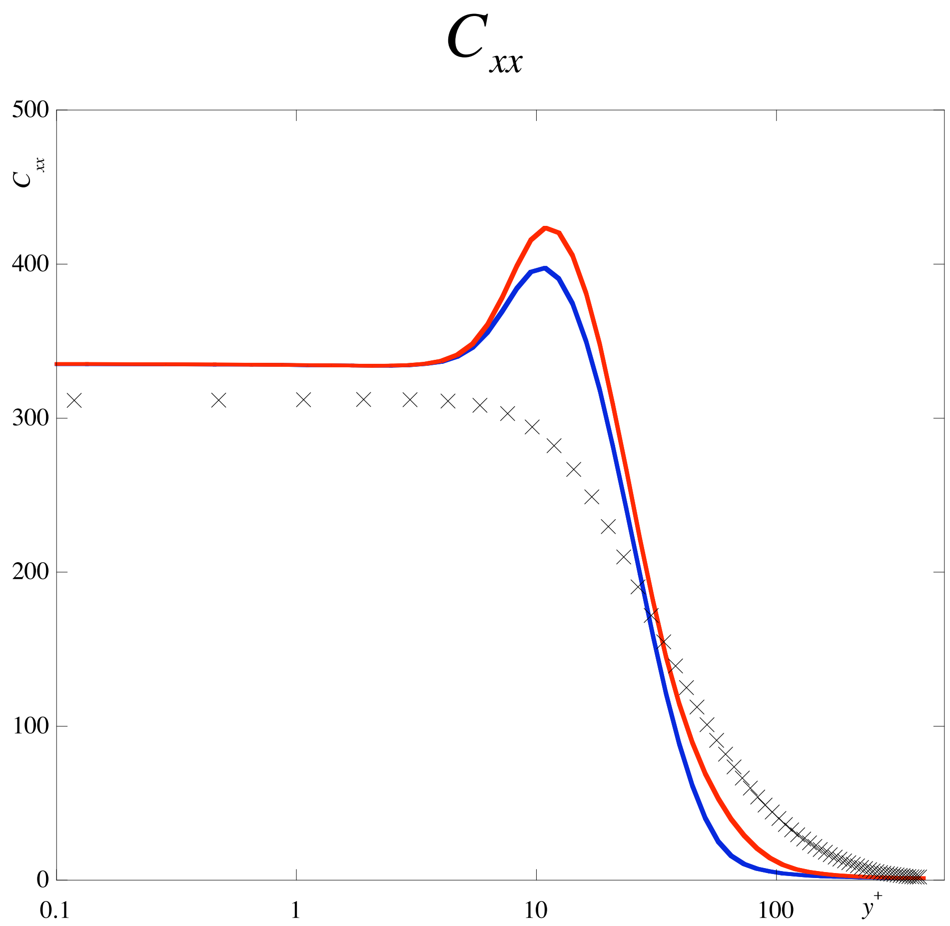


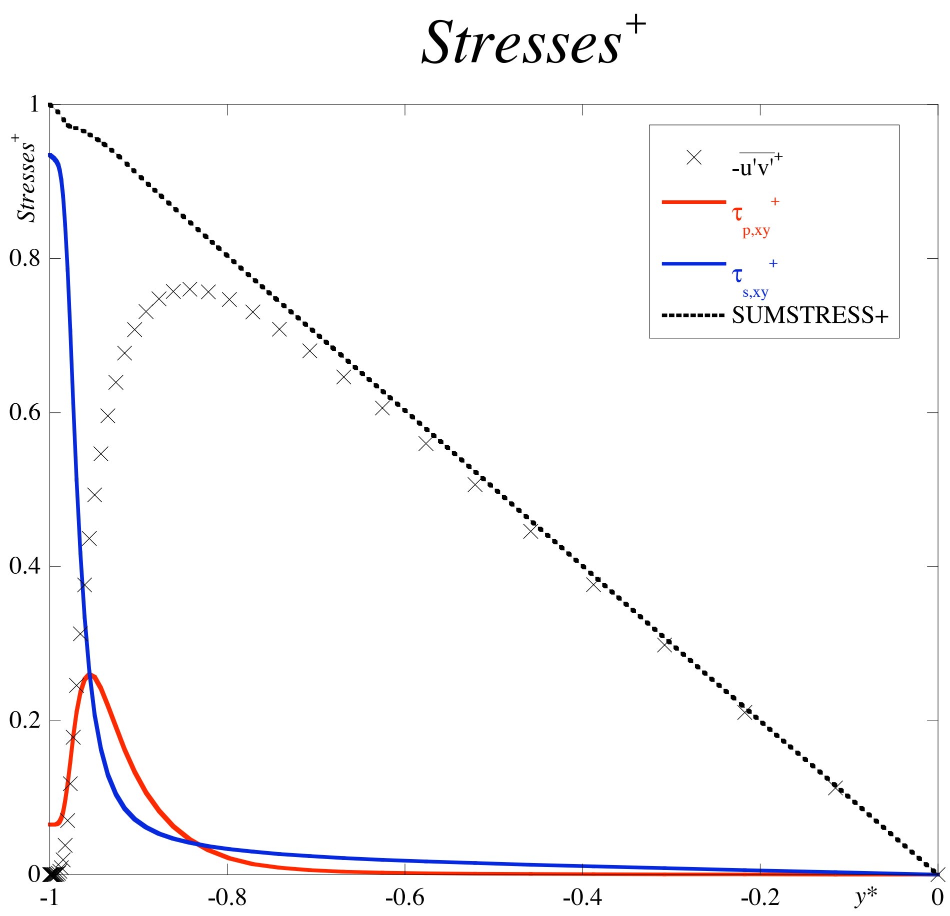
Some results 5: $Re_{\tau 0}$= 395; $We_{\tau 0}$= 25; β=0.9, L^2=900





Some results 6: $Re_{\tau 0}$= 395; $We_{\tau 0}$= 25; β=0.9, L^2=900

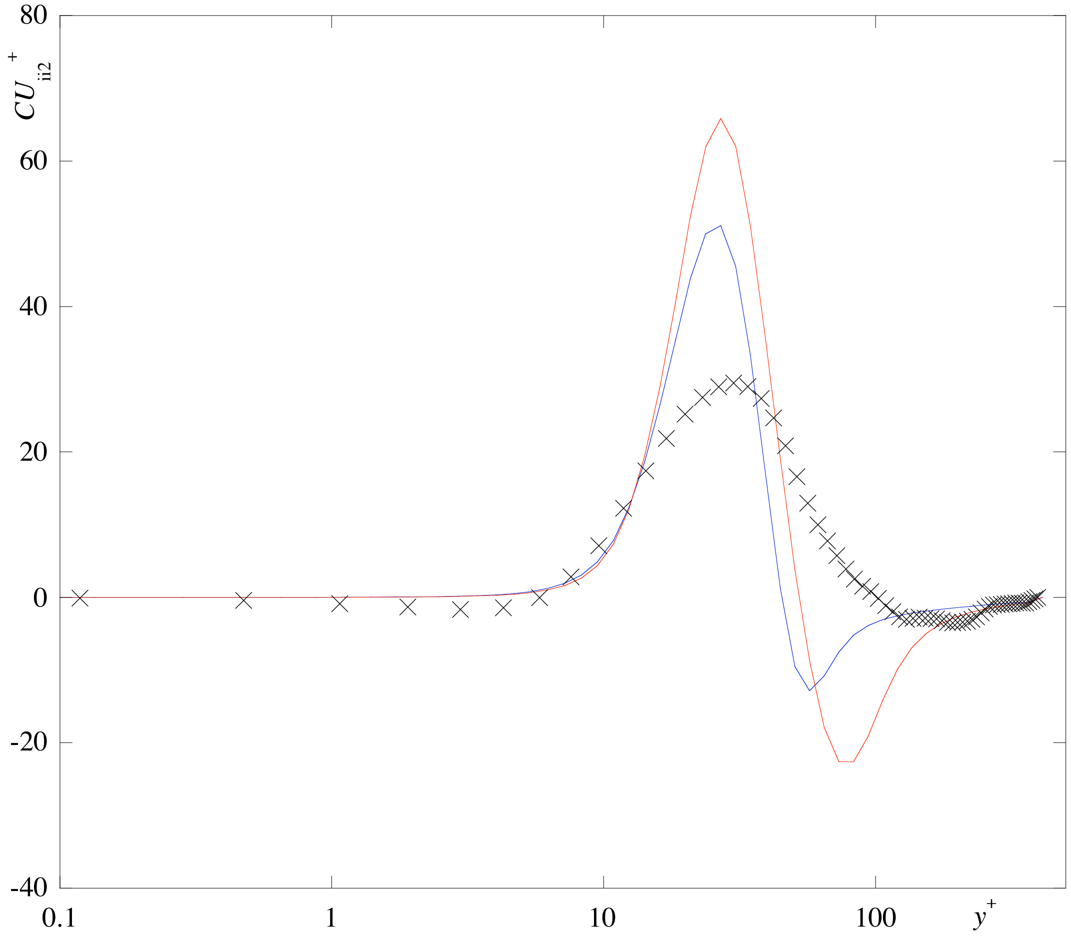




$$f\left(C_{kk}\right)C_{xx} = 2\lambda C_{xy}\frac{dU}{dy} + \lambda NLT_{xx} + 1$$

Some results 7: $Re_{\tau 0}$= 395; $We_{\tau 0}$= 25; β=0.9, L^2=900

$$CU^+_{iiy}$$



Conclusions

- Developed simplified k-ε model: code and closures are working
- Viscoelastic stress power well modeled by NLT_{ij}
- Viscoelastic turbulent transport (CU_{ijk}) is not that relevant at 18%
- NLT_{ij} is also required for C_{ij}

-Closure for NLT_{ij} has deficiencies and needs significant improvement
- Excessive dissipation of turbulence
- Need to model viscoelastic turbulence production close to wall
- Isotropic turbulence does not allow a good model
- Need to consider anisotropic turbulence: anisotr. k-ε and RSM

- Closure for CU_{ijk} is fair but also needs improvement: small impact