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# A New Perspective for Sizing of Distributed Generation and Energy Storage for Smart Households under Demand Response

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#### Abstract

12 As a recently increasing trend among different applications of smart grid vision, smart households as a new implementation area of demand 13 response (DR) strategies have drawn more attention both in research and in engineering practice. On the other hand, optimum sizing of 14 renewable energy based small scale hybrid systems is also a topic that is widely covered by the existing literature. In this study, the sizing of 15 additional distributed generation (DG) and energy storage systems (ESSs) to be applied in smart households, that due to DR activities have a 16 different daily demand profile compared with normal household profiles, is investigated. To the best knowledge of the Authors this is the first 17 attempt in the literature to investigate this issue, also including step-wise decreasing cost functions for DG and ESS, varying load and DG 18 production profiles seasonally, and weekday-weekend horizons for a long-term analysis period. The study is conducted using a mixed-integer 19 linear programming (MILP) framework for home energy management system (HEM) modeling and techno-economical sizing. Also, different 20 sensitivity analyses considering the impacts of variation of economic inputs on the provided model are realized.

31 Keywords: Distributed Generation; Energy Storage; Smart Households; Demand Response; Home Energy Management.

#### 23 Nomenclature 24 41.1

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25	A. Abbrev	lations
26	BCR	benefit-to-cost ratio.
27	DPP	discounted payback period.
28	DR	demand response.
29	ESS	energy storage system.
30	EV	electric vehicle.
31	PV	photovoltaics.
32	ТС	total cost.
33	TNPV	total net present value.
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35	B. Indices	
36	n	index of years in total project horizon
37	t	period of the day index in time units [h or min].
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39	C. Parame	eters
40	$C_{cap.ESS}$	ESS unit overnight capital cost [\$/kWh].

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41	$C_{cap,PV}$	PV unit overnight capital cost [\$/kW].
42	$C_{main.ESS}$	ESS unit annual maintenance cost [\$/kWh-y].
43	$C_{main,PV}$	PV unit annual maintenance cost [\$/kW-y].
44	$C_{rep.ESS}$	ESS unit replacement cost [\$/kWh].
45	$C_{ren PV}$	PV unit replacement cost [\$/kW].
46	$CE_{ESS}$	charging efficiency of the ESS.
47	$CE_{EV}$	charging efficiency of the EV.
48	$CR_{ESS}$	charging rate of the ESS [kW per time interval].
49	$CR_{FV}$	charging rate of the EV [kW per time interval].
50	d	real discount rate.
51	$DE_{FSS}$	discharging efficiency of the ESS.
52	$DE_{FV}$	discharging efficiency of the EV.
53	$DR_{ESS}^{DV}$	discharging rate of the ESS [kW per time interval].
54	$DR_{EV}$	discharging rate of the EV [kW per time interval].
55	$ESS_{ren flag}^{n}$	ESS replacement flag throughout project horizon.
56	$K_T$	number of time intervals in one hour.
57	$n_{FSSmax}$	maximum multiplication coefficient for ESS sizing considering base size (1 kWh in this study).
58	$N_{P}$	project horizon [vears].
59	n <sub>PV max</sub>	maximum multiplication coefficient for PV sizing considering base size (1 kW in this study).
60	$N_1, N_2$	modeling constants for ESS.
61	$N_2$	maximum power that can be drawn from the grid [kW].
62	$N_{4}$	maximum power that can be sold back to the grid [kW].
63	$P_t^{other}$	household power demand [kW].
64	P. <sup>PV,pro</sup>	nower produced by the PV [kW]
65	$PV^n$	PV replacement flag throughout project horizon
66	SOFESS,ini	initial state of energy of the ESS [kWh]
67	SOE SOFESS,max	maximum allowed state-of-energy of the ESS [kWh]
68	SOF ESS, min	minimum allowed state-of-energy of the ESS [kWh]
60	SOE SOE <sup>EV,ini</sup>	initial state of energy of the EV [kWh]
70	SOE	maximum allowed state-of-energy of the EV [kWh]
70	SOE <sup>EV,min</sup>	minimum allowed state of energy of the EV [kWh].
72	$T^a$	arrival time of EV to household
73	T T <sup>d</sup>	departure time of EV from household
74	TC.	total cost for the base case [\$]
75	1 Obase 1 <sup>buy</sup>	$r_{i}$ and $r_{i}$ and $r_{i}$ and $r_{i}$ and $r_{i}$
75	λ <sub>t</sub> sell	price of energy sold heals to the grid [cents/k wh].
70	$\lambda_t$	price of energy solu back to the grid [cents/k wil].
//		
78	D. Variable	25
79	$C_{cap,tot}$	total overnight capital investment cost [\$].
80	$C_{main.tot}$	total annual maintenance cost [\$].
81	$C_{rep.tot}$	total replacement cost [\$].
82	$n_{FSS}$	optimum size of ESS to be installed [kWh].
83	$n_{PV}$	optimum size of PV to be installed [kW].
84	$P_t^{ESS,ch}$	ESS charging power [kW].
85	P. ESS, dis	ESS discharging power [kW]
86	P <sup>ESS</sup> ,sold	nower injected to grid from the ESS [kW]
00 07	LESS,used	power injected to grid from the ESS [kw].
0/	$P_t$ $p^{EV.ch}$	Diversion and the satisfy household load from the ESS [kw].
88	$P_t$	Ev charging power [kw].
89	$P_t^{\rm LV,aus}$	EV discharging power [kW].
90	$P_t^{Lv,sola}$	power injected to grid from the EV [kW].
91	$P_t^{EV,used}$	power used to satisfy household load from the EV [kW].
92	$P_t^{grid}$	power supplied by the grid [kW].
93	$P_{t}^{PV,sold}$	power injected to grid from the PV [kW].
94	P. <sup>PV,used</sup>	nower used to satisfy household load from the PV [kW]
95	⁺t psold	total nower injected to the grid [kW]
50	• t	tour power injected to the grid [K 1].

96	$SOE_t^{ESS}$	state-of-energy of the ESS [kWh].
97	$SOE_t^{EV}$	state-of-energy of the EV [kWh].
98	$TC_{com}$	total cost for compared case [\$].
99	TCR	total cost reduction [\$].
100	$TPV_{inc}$	total present value of the income [\$].
101	TPV <sub>out</sub>	total present value of the outflow [\$].
102	$u_t^{ESS}$	binary variable. 1 if ESS is charging during period t, 0 else.
103	$u_t^{EV}$	binary variable. 1 if EV is charging during period t, 0 else.
104	$u_t^{grid}$	binary variable. 1 if grid is supplying power during period t, 0 else.
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#### 106 **1. Introduction**

107 *1.1. Motivation and background* 

Smart grid vision is one of the primary concerns of recent investments in electricity industry that is promoted by the shortterm and long-term plans of leading country governments. As the smart grid idea is mainly based on accommodating all types of generation and storage options and especially enabling active participation of consumer side of the generation/consumption balance, activities related to the demand side of the power system are gaining more importance [1]. Among these activities, demand response (DR) strategies play the major role in promoting the smart grid implementations [2].

The US Department of Energy (DOE) defines DR as "changes in electric usage by end-use customers from their normal consumption patterns in response to changes in the price of electricity over time, or to incentive payments designed to induce lower electricity use at times of high wholesale market prices or when system reliability is jeopardized". DR comprises incentive based programs and price based programs (time-of-use, critical peak pricing, dynamic pricing, etc.) [3,4]. DR can be considered mature for industrial consumers, but is a new concept for residential units responsible for nearly 40% of the global energy consumption [5]. The application of DR in such residential units calls for the definition of smart households that can monitor their use of electricity in real-time and act in order to lower their electricity bills [5,6].

120 DR activities for smart households surely result in a small or significant change in their daily power consumption pattern. The 121 home energy management (HEM) systems of smart households are likely to shift most of the possible consumption from peak 122 price periods to off-peak price periods (that is usually after midnight) in order to reduce the corresponding daily electricity 123 consumption cost [7]. Such shifting actions in DR based smart households are the main reason for the aforementioned changes 124 in daily power consumption profile. These changes raise concerns and points that require reconsideration such as the impact of 125 having new peaks in formerly off-peak hours etc. In this regard, sizing approaches for the evaluation of investments of small-126 scale generation and storage units at the end-users premises, considering only normal load patterns, should be reconsidered. DR 127 strategies and their impact on the load profile are likely to affect the technically and economically optimal results related to such 128 investments. This is a topic that requires attention since effective investments determine the development of distributed 129 generation, a core element of the future smart grid.

# 130 *1.2. Literature overview*

131 There is a rich literature on sizing of different hybrid distributed generation system structures for applying both in grid-132 connected and stand-alone modes of operation. As an example for sizing of stand-alone systems, Kolhe [8] provided the 133 optimum sizing of a stand-alone PV-battery hybrid system using levelized energy cost computation. Katsigiannis et al. [9] 134 applied a mixed simulated annealing-tabu search based optimization methodology for component sizing of a small autonomous 135 power system including wind turbine, PV, biodiesel, conventional diesel, fuel cell and battery systems. Hong and Lian [10] 136 employed a Markov-based genetic algorithm in order to techno-economically size the components of a stand-alone 137 wind/PV/diesel hybrid structure. A pattern search- based optimization method combined with a sequential Monte Carlo 138 simulation approach was proposed by Arabali et al. [11] for the stochastic performance assessment and sizing of a hybrid power 139 system including wind, PV and ESS units. A new perspective also considering the aging-based performance degradation impacts 140 on sizing results was presented by Erdinc and Uzunoglu in [12].

141 The sizing of renewable energy systems and ESS units in a grid-connected mode of operation has also been well-covered in 142 the existing literature. In this concept, Alsayed et al. [13] realized the optimum sizing of a grid-connected wind-PV hybrid 143 system adopting different multicriteria decision analysis optimization approaches. Bahramirad et al. [14] specifically focused on 144 ESS sizing for a microgrid with consideration of reliability constraints in mixed-integer linear programming (MILP) framework. 145 The same topic of ESS sizing in a MILP framework for a microgrid was also the topic of Chen et al. [15] from a different 146 perspective based on cost-benefit analysis for both islanded and grid-connected modes of operation. A significantly detailed 147 literature survey on different methods, several considerations, etc. applied for sizing of renewable energy based hybrid systems 148 was given in [16-20].

149 There are also many recent studies dealing with DR strategies for the optimum appliance operation of smart households. Chen 150 et al. [21] and Tsui and Chan [22] developed an optimization strategy for the effective operation of a household with a price 151 signal based DR. Li and Hong [23] proposed a "user-expected price" based DR strategy for a smart household also including a 152 battery based ESS aiming at lowering the total electricity cost by charging and discharging the ESS at off-peak and peak price 153 periods, respectively. However, the impact of including an additional EV load that can also be helpful for peak clipping in 154 certain periods when EV is at home and the possibility of an own production facility are not evaluated in Ref. [23]. Zhao et al. 155 [24] considered the HEM strategy based control of a smart household including photovoltaic (PV) based production facilities, 156 the availability of the EV and an ESS. However, V2H and further possible V2G operating modes of EV are not taken into 157 account in Ref. [24]. Restegar et al. [25] developed a smart home load commitment strategy considering all the possible 158 operating modes of EV and ESS, yet neglecting the impact of an extra peak power limiting strategy that is probable to be 159 imposed by a LSE. This is an important fact that is also disregarded in [21]-[24].

160 Pipattanasomporn et al. [26] and Kuzlu et al. [27] presented a HEM strategy considering peak power limiting DR strategy for 161 a smart household, including both smart appliances and EV charging. Shao et al. [28] also investigated EV for DR based load 162 shaping of a distribution transformer serving a neighborhood. Refs. [26]-[28] did not provide an optimum operating strategy 163 considering price variability with the aim of obtaining the lowest daily cost apart from just limiting the peak power drawn from 164 the grid by household in certain periods. Matalanas et al. [29] applied an HEM system based on neural networks with 165 experimental results for a household including PV and ESS. However, the impacts of varying price as well as other types of DR 166 strategies are not evaluated in Ref. [29]. Angelis et al. [30] performed the evaluation of a HEM strategy considering the 167 electrical and thermal constraints imposed by the overall power balance and consumer preferences. Chen et al. [31] provided an 168 appliance scheduling in a smart home considering dynamic prices and appliance usage patterns of consumer. Missaoui et al. [5] 169 also provided a smart building energy management strategy based on price variations and external conditions as well as comfort 170 requirements. The pricing data based energy management is also suggested by Hu and Li [32] together with a hardware 171 demonstration.

Besides, in a recent study, Erdinc [7] considered the possible operating conditions within a smart household including EV, ESS and PV under different DR strategies of price-based and peak-power limiting, where constant sizing of PV and ESS were considered and the sensitivity of total cost of daily operation of the household to PV and ESS sizes was considered manually without an optimization perspective.

176 These papers together with many other studies not referred here have provided valuable contributions to the application of 177 economical investments for small-scale renewable energy systems in general and smart grid concepts in household areas. 178 However, to the best knowledge of the authors none of the studies in the literature considered the sizing of extra renewable 179 energy system investments considering the changing load profile imposed by the price responsive DR activities within the 180 concept of smart households. One exception which can be considered the most similar area of research is the study of Kahrobaee 181 et al. [33], where the influence of demand side activities related to price variation were implemented within the sizing purpose of 182 a wind turbine and battery-based small own generation and ESS system for a smart household. However, in the proposed 183 strategy of Ref. [33], there were different steps where the optimum operating strategy of smart household appliances, ESS, etc. 184 was decided and the sensitivity of total daily operation cost of the household was evaluated in an optimization framework. 185 However, the combination of these different steps under a single step by a proper formulation can be considered more effective 186 to analyse the intercorrelated impacts of sizing and DR activities. Besides, only a single day operation was considered in 187 Ref. [33], where the impacts of seasonal, weekday-weekend impacts on load profiles as well as the variability of DG based power production throughout the year were neglected, which is the core of all sizing studies by providing at least 1 year of 188 189 system analysis.

# 190 *1.3. Contribution of the study*

The novel point of this study is the provision of a single step methodology to size additional PV and ESS for a smart household, the load profile of which is affected by the decisions of a HEM system that operates under dynamic pricing based DR.

Under a mixed-integer linear programming (MILP) modeling framework, the HEM structure and thus the daily operation of the smart household is associated with the sizing procedure, pertaining a long-term horizon. The HEM structure considers a small-scale distributed renewable energy generation system (PV), an electric vehicle (EV) capable of operating in vehicle-tohome (V2H) mode, together with an ESS.

Sizing of the PV and the ESS affects the smart household operation, while the load pattern induced by the DR scheme affects the sizing results. To reveal the relation of the aforementioned components, different case studies, as well as sensitivity analyses are presented. Besides, a step-wise decreasing unit capital cost function for PV and ESS is used to consider the cost advantage that arises with increased capacity, which is neither considered in many studies on sizing issue nor in the most similar study in the literature given in Ref. [33]. Moreover, the seasonal and weekday-weekend load variability is also taken into account together with EV availability variation for different household owner profiles.

# 204 1.4. Paper organization

The remainder of this paper is organized as follows: Section 2 gives the methodology employed in the study. Section 3 includes the case studies and sensitivity analyses for the evaluation of the sizing results for a smart-household participating in a DR initiative. Finally, concluding remarks are presented in Section 4.

# 208

# 209 2. System description and methodology

210 The objective is to minimize the total net present value (TNPV) of the cash flows:

$$Min. TNPV = TPV_{out} - TPV_{inc} (1)$$

which in turn aims maximizing the "Benefit-to-Cost Ratio (BCR)" expressed by (2) by trying to simultaneously maximizing  $TPV_{inc}$  and minimizing  $TPV_{out}$  in (1):

$$BCR = \frac{TPV_{inc}}{TPV_{out}}$$
(2)

In (1) and (2),  $TPV_{out}$  stands for the total present value of the outflows related to the total capital investment, replacement and maintenance costs of the additional PV based distributed generation (DG) and battery based ESS equipments for the total project lifetime and is calculated by:

$$TPV_{out} = C_{cap,tot} + C_{rep,tot} + C_{main,tot}$$
(3)

216 where C<sub>cap,tot</sub>, C<sub>rep,tot</sub> and C<sub>main,tot</sub> respectively stand for total capital, replacement and maintenance costs and are calculated

217 by (4)-(6):

$$C_{cap,tot} = C_{cap,PV} \cdot n_{PV} + C_{cap,ESS} \cdot n_{ESS}$$
(4)

$$C_{rep,tot} = \sum_{n=1}^{N_P} \left( \frac{PV_{rep,flag}^n \cdot C_{rep,PV} \cdot n_{PV}}{(1+d)^n} + \frac{ESS_{rep,flag}^n C_{rep,ESS} \cdot n_{ESS}}{(1+d)^n} \right)$$
(5)

$$C_{main,tot} = \sum_{n=1}^{N_P} \frac{C_{main,PV} \cdot n_{PV} + C_{main,ESS} \cdot n_{ESS}}{(1+d)^n}$$
(6)

where  $C_{cap,PV}$  and  $C_{cap,ESS}$  are PV and ESS capital costs,  $C_{rep,PV}$  and  $C_{rep,ESS}$  are PV and ESS replacement costs,  $C_{main,PV}$  and  $C_{main,ESS}$  are PV and ESS maintenance costs,  $n_{PV}$  and  $n_{ESS}$  are multiplication coefficients for PV and ESS sizing considering base size (1 kW and 1 kWh respectively),  $PV_{rep,flag}$  and  $ESS_{rep,flag}$  are PV and ESS replacement flags throughout project horizon, *d* is the real discount rate, and *n* is the year in  $N_P$  total project horizon (usually considered as 20 years for the economic lifetime of a renewable energy investment). It should be noted that capital cost is valid only for year zero while the period of maintenance cost starts with the first year (n=1) and replacement cost is only available for the periodical years when the usable lifetime of unit *i* ends that is considered by PV and ESS replacement flags.

On the other hand, in (1),  $TPV_{inc}$  represents the total present value of the incomes related to the annual total cost reduction (*TCR*) obtained in the total yearly cost of electricity consumption (*TC*) of the household by the additional benefits of several factors such as adding PV and ESS and also including DR for the total project lifetime and is calculated by:

$$TPV_{inc} = \sum_{n=0}^{NP} \frac{TCR}{(1+d)^n}$$
(7)

where *TCR* is the difference between *TC* in base case (e.g. without additional PV and ESS) and *TC* in compared case, and accordingly calculated as:

$$TCR = TC_{base} - TC_{com} \tag{8}$$

Both the *TC* values for base ( $TC_{base}$ ) and compared ( $TC_{com}$ ) cases in (8) are calculated as the difference between the energy bought from the grid and the energy sold back to the grid by the household-owned assets that are able to provide energy (e.g. PV, ESS and EV which are considered to be available for base and compared cases) in year *n*. The price variables are time dependent, a fact that implies time varying prices for both bought and sold energy.

$$TC = \sum_{t} \left( \frac{P_t^{grid}}{K_T} \cdot \lambda_t^{buy} - \frac{P_t^{sold}}{K_T} \cdot \lambda_t^{sell} \right)$$
(9)

In (9),  $P_t^{grid}$  is the total power bought from the grid at time *t*, and  $P_t^{sold}$  is the total power sold back to the grid which comprises power values sold from PV, ESS and EV ( $P_t^{PV,sold}$ ,  $P_t^{ESS,sold}$  and  $P_t^{EV,sold}$ ). In this study we consider that the HEM system first sells energy from the PV, next from the ESS and finally from the EV battery.

The constraints presented below comprise the basic body of the HEM system operation. The model can be easily extended and adapted to other more specific implementations (e.g. by further modeling specific smart-appliances such as HVAC, water heaters, appliances with cycling operation and/or customer's contract details). Any time granularity can be used simply by selecting the appropriate  $K_T$ . For instance, for a 15-minute interval the  $K_T$  coefficient must be 4, as one hour comprises four 15minute intervals.

Equation (10) states that the load consisting of the residential load  $(P_t^{other})$ , the charging needs of the EV  $(P_t^{EV,ch})$  and the ESS  $(P_t^{ESS,ch})$  is either satisfied by the grid  $(P_t^{grid})$  or by the combined procurement of energy by the PV, the ESS and the EV  $(P_t^{PV,used}, P_t^{EV,used} \text{ and } P_t^{ESS,used})$ .

$$P_t^{grid} + P_t^{PV,used} + P_t^{EV,used} + P_t^{ESS,used} = P_t^{other} + P_t^{EV,ch} + P_t^{ESS,ch} \quad \forall t$$
(10)

Equation (11) enforces the fact that the actual power provided by the ESS discharge  $(P_t^{ESS,dis} \cdot DE_{ESS})$  can be used to cover a 245 portion of the household needs  $(P_t^{ESS,used})$  or injected back to the grid  $(P_t^{ESS,sold})$ . Constraints (12) and (13) are employed for 246 247 preventing a possible simultaneous charging and discharging operation. Constraints (14) and (15) impose a limit on the charging  $(P_t^{ESS,ch})$  and discharging  $(P_t^{ESS,dis})$  power of the ESS. The idle ESS state can be described by any of these constraints by the 248 249 time the respective power variable is allowed to have zero value. Equations (16)-(19) describe the state-of-energy of the ESS. Constraint (16) forces the state-of-energy at every interval  $(SOE_t^{ESS})$  to have the value that it had at the previous interval 250 251  $(SOE_{t=1}^{ES})$  plus the actual amount of energy that is transferred to the battery if it is charging at that interval minus the energy that 252 is subtracted if the battery is discharging during that interval. At the beginning of the time horizon the state-of-energy of the ESS coincides with the initial state-of-energy of the ESS (SOE<sup>ESS,ini</sup>), as described by Eq. (17). Constraint (18) limits the state-of-253 254 energy of the battery to be less than the ESS capacity (SOE<sup>ESS,max</sup>). Similarly, constraint (19) prevents the deep discharge of the battery by imposing a least state-of-energy limit (SOEESS,min). Lastly, constraint (20) limits the multiplication coefficient to be 255 256 below an upper limit for ESS.

$$P_t^{ESS,used} + P_t^{ESS,sold} = P_t^{ESS,dis} \cdot DE_{ESS} \,\forall t \tag{11}$$

$$P_t^{ESS,ch} \le N_1 \cdot u_t^{ESS} \ \forall t \tag{12}$$

$$P_t^{ESS,dis} \le N_2 \cdot (1 - u_t^{ESS}) \,\forall t \tag{13}$$

$$P_t^{ESS,ch} \le CR_{ESS} \cdot n_{ESS} \ \forall t \tag{14}$$

$$P_t^{ESS,dis} \le DR_{ESS} \cdot n_{ESS} \ \forall t \tag{15}$$

$$SOE_t^{ESS} = SOE_{t-1}^{ESS} + CE_{ESS} \cdot \frac{P_t^{ESS,ch}}{\kappa_T} - \frac{P_t^{ESS,dis}}{\kappa_T} \quad \forall t \ge 1$$
(16)

$$SOE_t^{ESS} = SOE^{ESS,ini} \cdot n_{ESS} \ if \ t = 1$$
 (17)

$$SOE_t^{ESS} \le SOE^{ESS,max} \cdot n_{ESS} \quad \forall t$$
 (18)

$$SOE_t^{ESS} \ge SOE^{ESS,min} \cdot n_{ESS}, \ \forall t$$
 (19)

$$n_{ESS} \le n_{ESS,max} \tag{20}$$

Equation (21) enforces the fact that the actual power provided by the EV discharge  $(P_t^{EV,dis} \cdot DE_{EV})$  can be used to cover a 257 portion of the household needs ( $P_t^{EV,used}$ ) or injected back to the grid ( $P_t^{EV,sold}$ ). Constraints (22) and (23) impose a limit on the 258 charging  $(P_t^{EV,ch})$  and discharging  $(P_t^{EV,dis})$  power of the EV. The idle EV state can be described by any of these constraints by 259 260 the time the respective power variable is allowed to have zero value. Equations (24)-(28) describe the state-of-energy of the EV. Constraint (24) forces the state-of-energy at every interval ( $SOE_t^{EV}$ ) to have the value that it had at the previous interval 261  $(SOE_{t-1}^{EV})$  plus the actual amount of energy that is transferred to the EV battery if it is charging at that interval minus the energy 262 263 that is subtracted if the EV battery is discharging during that interval. At the arrival time of EV to household, the state-of-energy of the EV coincides with the initial state-of-energy of the EV (SOEEV,ini), as described by Eq. (25). Constraint (26) limits the 264 state-of-energy of the EV battery to be less than its capacity (SOE<sup>EV,max</sup>). Similarly, constraint (27) prevents the deep discharge 265 266 of the EV battery by imposing a least state-of-energy limit (SOE<sup>EV,min</sup>). Eq. (28) represents the issue of having the EV battery 267 fully charged in departure time of EV in the morning. Finally, Eq. (29) ensures that all the variables related to EV modeling are zero apart from the time interval between arrival time of EV to household  $(T^a)$  and departure time of EV from household  $(T^d)$ . 268

$$P_t^{EV,used} + P_t^{EV,sold} = P_t^{EV,dis} \cdot DE_{EV} \ \forall t \in [T^a, T^d]$$
(21)

$$P_t^{EV,ch} \le CR_{EV} \cdot u_t^{EV} \,\forall t \in [T^a, T^d]$$

$$\tag{22}$$

$$P_t^{EV,dis} \le DR_{EV} \cdot (1 - u_t^{EV}) \,\forall t \in [T^a, T^d]$$

$$\tag{23}$$

$$SOE_t^{EV} = SOE_{t-1}^{EV} + CE_{EV} \cdot \frac{P_t^{EV,ch}}{K_T} - \frac{P_t^{EV,dis}}{K_T} \quad \forall t \in [T^a, T^d]$$
(24)

$$SOE_t^{EV} = SOE^{EV,ini} \quad if \ t = T^a \tag{25}$$

$$SOE_t^{EV} \le SOE^{EV,max} \quad \forall t \in [T^a, T^d]$$
 (26)

$$SOE_t^{EV} \ge SOE^{EV,min} \quad \forall t \in [T^a, T^d]$$
 (27)

$$SOE_t^{EV} = SOE^{EV,max} \quad if \ t = T^d \tag{28}$$

$$SOE_t^{EV} = P_t^{EV,used} = P_t^{EV,sold} = P_t^{EV,dis} = P_t^{EV,ch} = 0 \quad \forall t \notin [T^a, T^d]$$
(29)

Similarly to Eqs. (11) and (21), Eq. (30) enforces the fact that the actual power provided by the PV  $(P_t^{PV,pro})$  can be used to cover a portion of the household needs  $(P_t^{PV,used})$  or injected back to the grid  $(P_t^{PV,sold})$ . Lastly, similar to (20), constraint (31) limits the multiplication coefficient to be below an upper limit for PV.

$$P_t^{PV,used} + P_t^{PV,sold} = P_t^{PV,pro} \cdot n_{PV}, \quad \forall t$$
(30)

$$n_{PV} \le n_{PV,max} \tag{31}$$

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The total amount of power injected to the grid  $(P_t^{sold})$  consists of the amount of power provided by the PV  $(P_t^{PV,sold})$ , the ESS  $(P_t^{ESS,sold})$  and the EV  $(P_t^{EV,sold})$  as mentioned before. This is enforced by Eq. (32).

$$P_t^{sold} = P_t^{PV,sold} + P_t^{ESS,sold} + P_t^{EV,sold}, \quad \forall t$$
(32)

Equations (33) and (34) implement the logic of power exchange. If power from the grid is needed to be drawn, then it is not possible to inject power back to the grid. The reverse case is also described by these constraints.  $N_3$  is a positive integer value that imposes a limitation on the power that can be drawn from the grid. This limitation may represent a restriction posed by the aggregator or the responsible entity for the end-user electrification in order to face the situation where in its control area exist multiple households that own HEM system. The implementation of a time-varying peak power drawn from the grid limit as a different DR strategy can be easily adapted on this formulation, by replacing the  $N_3$  by a time-dependent parameter. Similarly,  $N_4$  imposes a limit on the power that can be injected back to the grid and also can be replaced by a time-dependent parameter.

$$P_t^{grid} \le N_3 \cdot u_t^{grid}, \quad \forall t \tag{33}$$

$$P_t^{sold} \le N_4 \cdot (1 - u_t^{grid}), \quad \forall t \tag{34}$$

Different consumer options and behavioral details can be expressed by fixing the charging and discharging variables of the ESS and EV to be zero in the appropriate time intervals. Different policies (e.g. energy selling back options) can be modeled by fixing the selling energy/power variables to zero or other desired values.

## 284 **3. Test and Results**

To evaluate the sizing of additional PV and ESS investment for the smart household case including a DR-based changing demand pattern, the MILP model is tested in GAMS v.24.1.3 using the solver CPLEX v.12 [34] and the obtained case studies based results are discussed in this section. The household load demand is provided considering power values of real household appliances given in [35] for a smart home demonstration project. The utilized appliance data are presented in Table 1. Three case studies dealing with different household owner profiles are evaluated in this study:

291 **Case-1:** A 4-people family where there is a housewife that is all at home in weekdays.

292 **Case-2:** A 4-people family where both parents work and no one is at home in day time within weekdays.

293 **Case-3:** A single person that works within weekdays.

The obtained total household demand variation apart from additional EV and ESS operation based load are given in Figs. 1-3 for different household owner profiles. It is to be noted that impacts of seasonal conditions and weekday-weekend are all considered as seen from Figs. 1-3 to obtain a more realistic yearly load profile compared to the case of repeating 24 h of load demand for a single day to adjust to a yearly profile. It is also evident from the given power variations in Figs. 1-3 that the profile of household owner results in a considerable change in power pattern. Besides, Fig. 4 shows a real-time measured hourly average power production profile of a solar farm normalized to 1 kW base in 2013. This base power production profile is multiplied by  $n_{pv}$  value decided by sizing approach and accordingly adjusted to different kW power ratings for PV system.

A bi-directional EV operation including both V2G (meaning that EV sells energy back to the grid) and V2H (meaning that a portion of the energy stored in the EV battery is used to partly cover the household load) options can be considered. However, in order to better evaluate the sole impacts of additional PV and ESS installation, the V2G capability of EV is disabled as there will be case studies considering the impacts of increase in selling back flat rate that will directly increase also the sold back energy by EV via V2G.

The specifications of a Chevy Volt with a battery rating of 16 kWh are considered for the EV. The Chevy Volt is employed with a charging station limited to a charging power of 3.3 kW [36]. The same power limit is also assumed to be valid for the discharging operation in V2H mode. The charging and discharging efficiencies are considered 0.95. It is also considered that the initial EV battery energy is 8 kWh (50% state-of-energy) while arriving at home and the lower limit of EV state-of-energy is restricted to 4.8 kWh (30% state-of-energy) to avoid deep-discharging. The departure and arrival times are considered as given in Table 2 related to different case studies. It should be noted that for all case studies, EV is assumed to be at home all day on Sundays.

The following assumptions hold for the ESS; its initial state-of-energy is 1/2 of the maximum battery energy capacity and charging/discharging efficiencies are 0.95. The charging and discharging limits are 0.2 of the maximum battery capacity. Lastly, the deep-discharging limit of battery based ESS is 1/4 of its maximum energy capacity.

316 Integrating the two-way energy transactions between the end-user and the utility, the net-metering approach is utilized.
317 When the available energy from the household-owned resources is sufficient to cover the total of the needs, the excess of energy

318 can be sold back to the grid and vice versa. For pricing the bought energy from the grid, a dynamic pricing based DR scheme is 319 considered. The time-varying price signal available for the consumer via the smart meter is shown in Fig. 5 [22], which is 320 repeated to obtain data for 8760 h.

Besides, a constant flat rate is paid to the end-user for the energy sold-back to the grid. Payment of flat rates with net metering is an approach also used in practice in different countries. A dynamically changing rate for energy sold can also be easily applied within the provided formulation, as Eq. (6) is suitable both for considering flat and dynamic rates.

The capital cost data considered in this study related to sizing procedure are shown in Table 3 as decreasing step-wise functions denoting the cost advantage that arises with increased capacity. It is to be noted that PV and ESS sizes are bounded with upper limits of 10 kW and 10 kWh for this study. Any other upper limit can easily be applied considering roof area that PV can be applied, limit of volume dedicated to ESS installation, etc. The replacement cost of PV and battery are considered as the same as the capital costs and maintenance costs are assumed as 5% of capital cost in a yearly period. Besides, the replacement time of PV and ESS are considered as 20 and 10 years, respectively. Moreover, the real discount rate is assumed as 0.05 and project lifetime is taken into account as 20 years.

331 The results for the above given economic data considering DR activities based load pattern of the smart household are 332 presented below.

The sizing results for different case studies together with the impacts of reduction in PV and ESS unit costs in comparison with changes in energy selling back flat rate are evaluated in order to conduct a case analysis and sensitivity analysis together. The corresponding results are presented in Tables 4-9 for different cases. It should be noted that all the costs (installation, replacement, maintenance) are considered to decrease with the same ratio.

337 It is clear from the results that PV and ESS size increase with the increase of flat rate of selling energy back to grid and 338 decrease of individual costs as can be expected. Besides, it can be seen that if the algorithm decides that investment of PV and 339 ESS is feasible, maximum limit of PV and ESS size is provided as the optimum configuration as more the capacity of such 340 systems more the benefit is. The most profitable case is Case-2 as anyone is at home during the day and the load demand is 341 minimum when the PV production is at the highest, which ensures more energy can be sold to grid without the need of covering 342 a bigger household demand. This is especially more profitable when the flat rate to sell back energy is higher as HEM system 343 always tries to sell back more energy to grid to increase benefits. As the case of flat rate of 0.05 \$ and cost ratio of 50% provides 344 feasibility of both PV and ESS investment in all cases, this case is examined in more detail. This case results in a  $TPV_{inc}$  value of 15789.671 \$ and a TPV<sub>out</sub> value of 11703.332 \$ for Case-1, which in turn provides a BCR of nearly 1.35. As providing 345 346 results for the 8760 h of the yearly period is significantly detailed, for the easiness of tracking, a random day is selected and the 347 related results are presented from Case-1 under the conditions of flat rate of 0.05 \$ and cost ratio of 50%.

For the date of 02.01.2013, the injected to grid and used power from PV system together with total production is presented in Fig. 6. It is observed that some of the produced energy by PV is injected back to the grid while a portion is utilized within the smart household in the evaluated sample case.

The battery based ESS power decomposition and the corresponding energy variation is shown in Figure 7. As seen, ESS provides a cycling based operation that stores energy and then sells back to grid or utilized this stored energy within household during higher price periods. Especially, if the time 7 pm which is the highest price period during the day time (see Figure 5) is examined, the ESS discharges till the maximum discharging power limit and accordingly helps to cover the household's load, as expected in order to reduce the power procurement from the grid in such a high price period.

A similar issue is also noticed within the EV power decomposition and energy variation shown in Figure 8. EV battery is charged and discharged considering price variations. As also seen, for the time of departure from home, EV battery is fully charged as requested. The periods between 8 am and 5 pm are idle periods when EV is not at home, thus all the power values are zero for this periods. The energy is shown as 8 kWh (initial energy level assumed when EV returns back home) for simplification in these periods but this is not totally known as the EV is not at home in these hours and the exact utilization periods for driving are not accordingly available for HEM system.

As the flat rate of selling back energy is always greater than price of buying energy from the grid, the case that total EV and ESS power values are greater than load demand means the rest of the energy is injected back to grid with this higher price when grid power is surely zero as load is covered by total of EV and ESS. However, such a condition is not always possible for lower flat rates of selling back energy as the algorithm decides the proper operation of each hour considering the individual values of buying and selling price of energy.

# 367 4. Conclusions

368 In this study, a MILP model for techno-economic optimum sizing of additional PV and ESS investment for a DR-based HEM 369 system controlled smart household was provided. The novelty of this paper lies in the consideration of the notably changing load 370 pattern due to DR activities, an important issue that has not been treated by the existing research studies. Besides, as an issue 371 that is not considered in the broad part of literature on sizing, the impacts of increment in size of PV and ESS on unit costs are 372 taken into account with a step-wise decreasing cost function. It is clear from the obtained results that considering DR based load 373 pattern changes significantly the sizing results and thus such investments for new generation residential areas should cover this 374 important impact during the planning phase. Additional case studies were also conducted to observe and present the sensitivity 375 of PV and ESS techno-economic sizing on unit costs and cost of selling back energy to the grid. Hence, a new insight to the 376 literature on sizing was given in this paper from a different perspective that can be promoted with new studies in the area.

- 379 formulation for the operation of more appliances, such as HVACs, electric heaters, water heaters, etc., which is the topic of a
- 380 future study of the authors. Besides, the further analysis of PV and ESS sizing sensitivity to different pricing scenarios apart
- 381 from a single dynamic daily profile, in order to provide a correlation map for aiding policy implications to promote smart grid
- 382 applications in end-user areas, is also planned as a future study of the authors.

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# **Figure Captions**

- Fig. 1. The household power profiles for Case-1.
- Fig. 2. The household power profiles for Case-2.
- Fig. 3. The household power profiles for Case-3.
- Fig. 4. The normalized power production for a 1 kW PV system.
- Fig. 5. The dynamic pricing data for DR activities within smart household.
- Fig. 6. The PV system power decomposition for the sample case.
- Fig. 7. The battery based ESS unit power decomposition and energy variation for the sample case.
- Fig. 8. The EV battery power decomposition and energy variation for the sample case.



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Fig. 1. The household power profiles for Case-1.



(g) Winter weekday profile.





Fig. 3. The household power profiles for Case-3.



Fig. 4. The normalized power production for a 1 kW PV system.



Fig. 5. The dynamic pricing data for DR activities within smart household.



Fig. 6. The PV system power decomposition for the sample case.



Fig. 7. The battery based ESS unit power decomposition and energy variation for the sample case.



Fig. 8. The EV battery power decomposition and energy variation for the sample case.

**Table Captions** Table 1. Household appliance data. Table 2. EV departure and arrival times for different case studies. Step-wise decreasing unit costs for PV and battery based ESS. Table 3. Case-1: Sensitivity of PV size to cost reduction and flat rate for selling energy back to grid. Table 4 Table 5 Case-1: Sensitivity of ESS size to cost reduction and flat rate for selling energy back to grid. Table 6 Case-2: Sensitivity of PV size to cost reduction and flat rate for selling energy back to grid. Table 7 Case-2: Sensitivity of ESS size to cost reduction and flat rate for selling energy back to grid. Table 8 Case-3: Sensitivity of PV size to cost reduction and flat rate for selling energy back to grid. Case-3: Sensitivity of ESS size to cost reduction and flat rate for selling energy back to grid. Table 9 

Table I. Household appliance da	<ol> <li>Household ar</li> </ol>	pliance data
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Appliance	Power [kW]
Oven	2.4
Cooker Hood	0.225
Microwave	1.2
Refrigerator	1.666
Washing Machine	1.4
Dishwasher	1.32
Iron	2.4
Toaster	0.8
Kettle	2
Hairdryer	1.8
Telephone	0.005
TV	0.083
Desktop Computer	0.15
Air Conditioner	1.14
Hair Straightener	0.055
Printer	0.011
Lighting	0.1
Other (Fixed)	0.05

Table 2. EV departure and arrival times for different case studies.

Season	Time of the week	Departure-Arrival	Case-1	Case-2	Case-3
	Waaliday	Departure	8am	8am	8am
Spring	weekday	Departure-ArrivalCase-1Case-2CaseDeparture8am8am8am8amArrival7pm5pm5pmDeparture9pm6pm9pmArrival11pm11pm12amDeparture8am9am8amArrival7pm5pm5pmDeparture8am9am8amArrival7pm5pm5pmDeparture2pm11am9pmArrival6pm7pm12amDeparture8am9am8amArrival6pm5pm5pmDeparture9pm2pm10ppArrival11pm5pm12amDeparture8am9am8amArrival11pm5pm12amDeparture8am9am8amArrival11pm5pm12amDeparture8am9am8amArrival6pm5pm5pmDeparture8pm2pm10ppArrival6pm5pm5pmDeparture8pm2pm10ppArrival11pm5pm12amDeparture8pm2pm10ppArrival11pm5pm12am	5pm		
Season Spring Summer Autumn Winter	Weekend (Seturday)	Departure	9pm	6pm	9pm
	weekend (Saturday)	kDeparture-ArrivalCase-1Case-1Departure8amArrival7pmPeparture9pmy)Departure9pmArrival11pmDeparture8amArrival7pmDeparture8amArrival7pmParture2pmArrival6pmDeparture8amArrival6pmDeparture8amArrival6pmDeparture9pmArrival11pmDeparture8amArrival6pmUpArrivalDeparture8amArrival11pmArrival6pmArrival11pm	11pm	12am	
	Waakday	Departure	arture-ArrivalCase-1Case-2CaseDeparture8am8am8amArrival7pm5pm5prDeparture9pm6pm9prArrival11pm11pm12aDeparture8am9am8arArrival7pm5pm5prDeparture8am9am8arArrival7pm5pm5prDeparture2pm11am9prArrival6pm7pm12aDeparture8am9am8arArrival6pm5pm5prDeparture9pm2pm10pArrival11pm5pm12aDeparture8am9am8arArrival6pm5pm5prDeparture8am9am8arArrival11pm5pm12aDeparture8am9am8arArrival6pm5pm5prDeparture8pm2pm10pArrival6pm5pm5prDeparture8pm2pm10pArrival11pm5pm12a	8am	
Summer	weekday	Arrival	7pm	5pm	5pm
	Weakand (Saturday)	Departure	2pm	11am	9pm
	weekend (Saturday)	Arrival	6pm	7pm	12am
	Waakday	Departure	8am	9am	8am
Autumn	weekday	Arrival	6pm	5pm	5pm
Autumn	Waakand (Saturday)	Departure	9pm	2pm	10pm
	weekend (Saturday)	Arrival	11pm	5pm	12am
	Waakday	Departure	8am	9am	8am
Winter	weekday	Arrival	6pm	5pm	5pm
w inter	Weekend (Saturday)	Departure	8pm	2pm	10pm
	weekend (Saturday)	Arrival	11pm	5pm	12am

Table 3. Step-wise decreasing unit costs for PV and battery based ESS.

Size interval (kW for PV, kWh for battery)	Unit cost for PV [\$/kW]	Unit cost for battery [\$/kWh]
0-1	1330	300
1-2	1300	290
2-3	1300	290
3-4	1270	270
4-5	1270	260
5-6	1210	260
6-7	1160	240
7-8	1150	230
8-9	1140	220
9-10	1120	200

		Fl	at rate i	for sellin	ng ener	gу	
		0.01	0.02	<b>Φ/Κ W Π</b>	0.04	0.05	
		0.01	0.02	0.05	0.04	0.05	
	50%	0	0	0	10	10	
PV cost ratio	60%	0	0	0	0	10	
	70%	0	0	0	0	0	
	80%	0	0	0	0	0	
	90%	0	0	0	0	0	
	100%	0	0	0	0	0	

Table 5. Case-1: Sensitivity of ESS size to cost reduction and flat rate for selling energy back to grid.

		Fl	at rate :	for selli [\$/kWh]	ng energ	gy
		0.01	0.02	0.03	0.04	0.05
	50%	0	0	0	0	10
ESS cost ratio	60%	0	0	0	0	0
	70%	0	0	0	0	0
	80%	0	0	0	0	0
	90%	0	0	0	0	0
	100%	0	0	0	0	0

Table 6. Case-2: Sensitivity of PV size to cost reduction and flat rate for selling energy back to grid.

		Fl	at rate :	for selli [\$/kWh]	ng energ	gy
		0.01	0.02	0.03	0.04	0.05
	50%	0	0	0	10	10
PV cost ratio	60%	0	0	0	0	10
	70%	0	0	0	0	10
	80%	0	0	0	0	0
	90%	0	0	0	0	0
	100%	0	0	0	0	0

Table 7. Case-2: Sensitivity of ESS size to cost reduction and flat rate for selling energy back to grid.

		Flat rate for selling energy [\$/kWh]					
		0.01	0.02	0.03	0.04	0.05	
	50%	0	0	0	0	10	
ESS cost ratio	60%	0	0	0	0	10	
	70%	0	0	0	0	0	
	80%	0	0	0	0	0	
	90%	0	0	0	0	0	
	100%	0	0	0	0	0	

Table 8. Case-3: Sensitivity of PV size to cost reduction and flat rate for selling energy back to grid.

		Flat rate for selling energy				
				[\$/kWh]		
		0.01	0.02	0.03	0.04	0.05
	50%	0	0	0	10	10
DV/	60%	0	0	0	0	10
PV	70%	0	0	0	0	10
cost ratio	80%	0	0	0	0	0
	90%	0	0	0	0	0
	100%	0	0	0	0	0

		Flat rate for selling energy [\$/kWh]				
		0.01	0.02	0.03	0.04	0.05
ESS cost ratio	50%	0	0	0	0	10
	60%	0	0	0	0	0
	70%	0	0	0	0	0
	80%	0	0	0	0	0
	90%	0	0	0	0	0
	100%	0	0	0	0	0